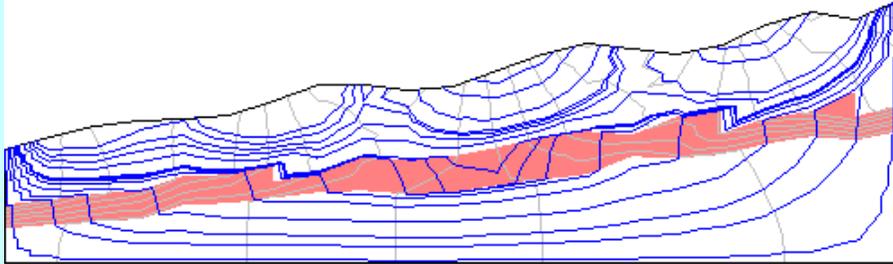
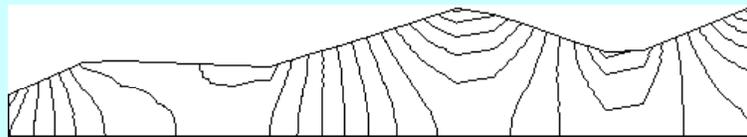


**UPPER BOUNDARY IS
CONSTANT HEAD**
EQUAL TO WATER TABLE ELEVATION
LIKE MANY RESERVOIRS PROVIDING AND RECEIVING WATER
no exaggeration -- head distribution
with aquitard

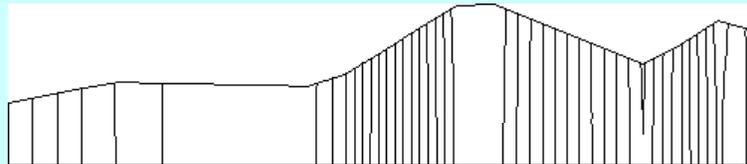


**NOTE THAT
POROSITY DOES NOT EFFECT FLOW FIELD
IT ONLY CHANGES TRAVEL TIME**

no exaggeration -- head distribution

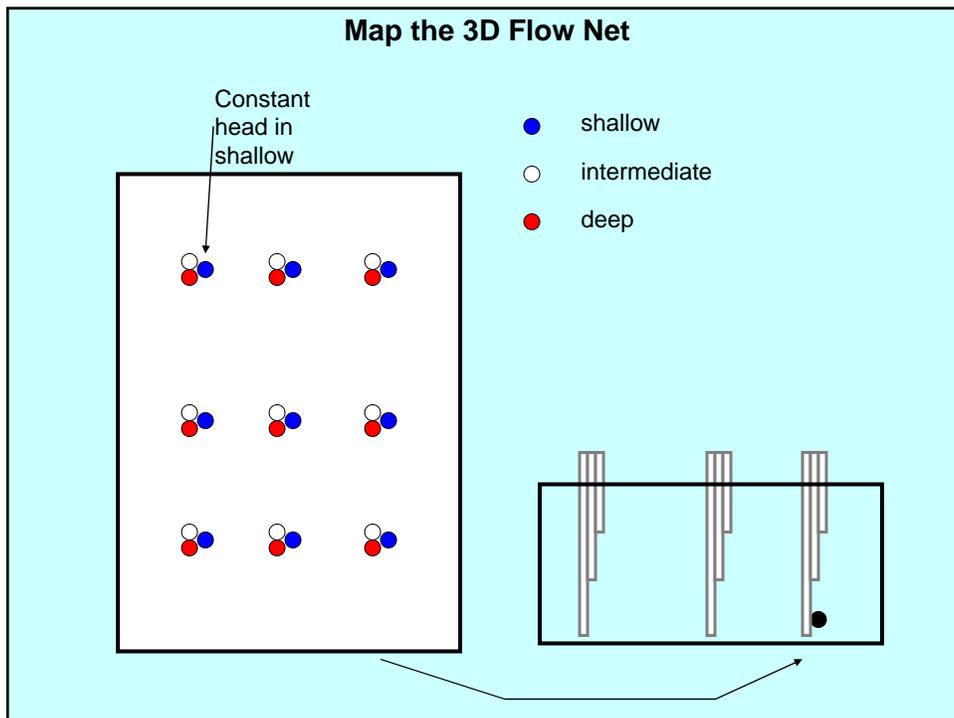
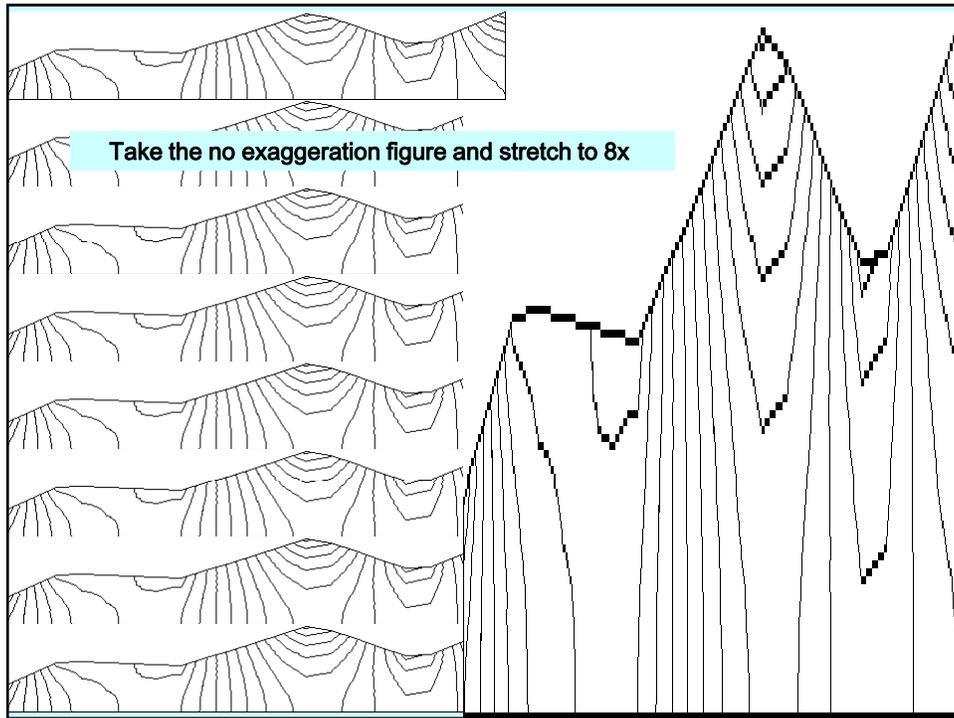


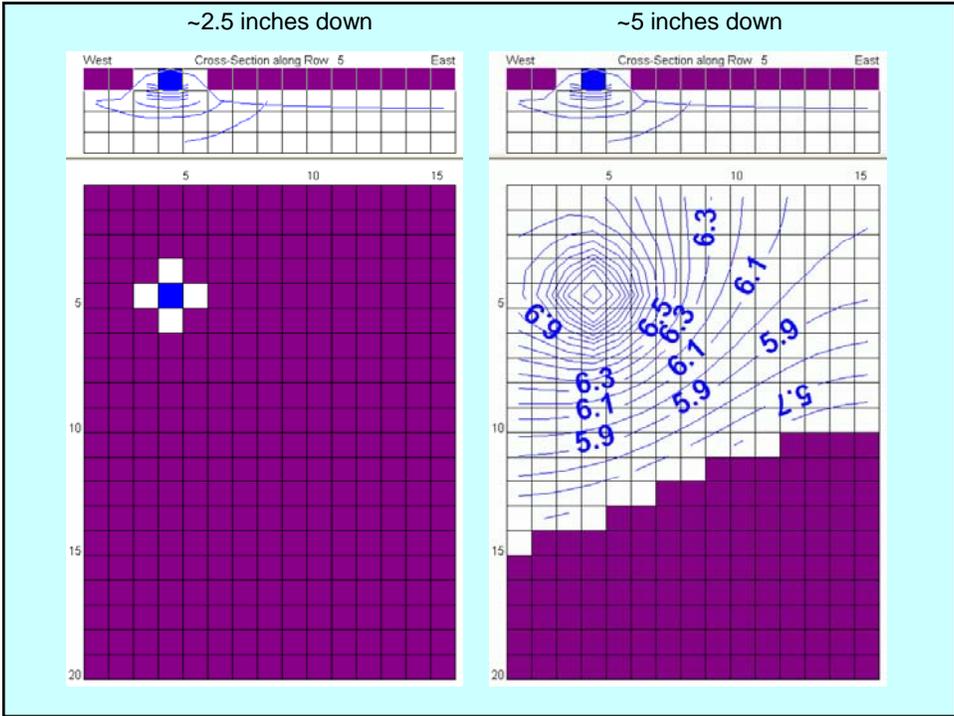
draw similar shape but under 10x exaggeration -- head distribution

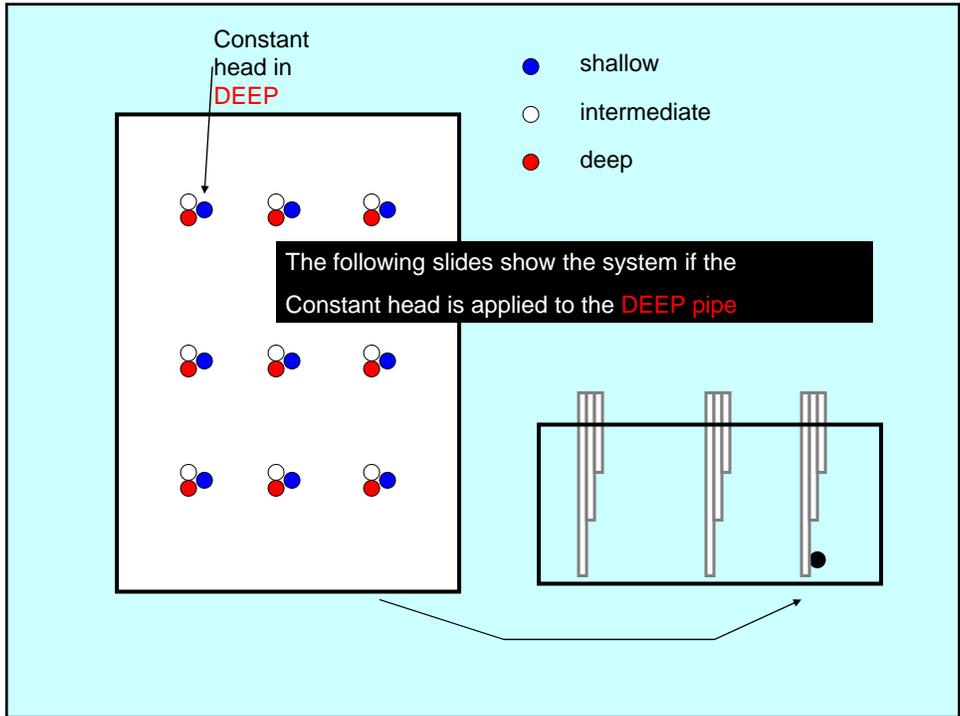
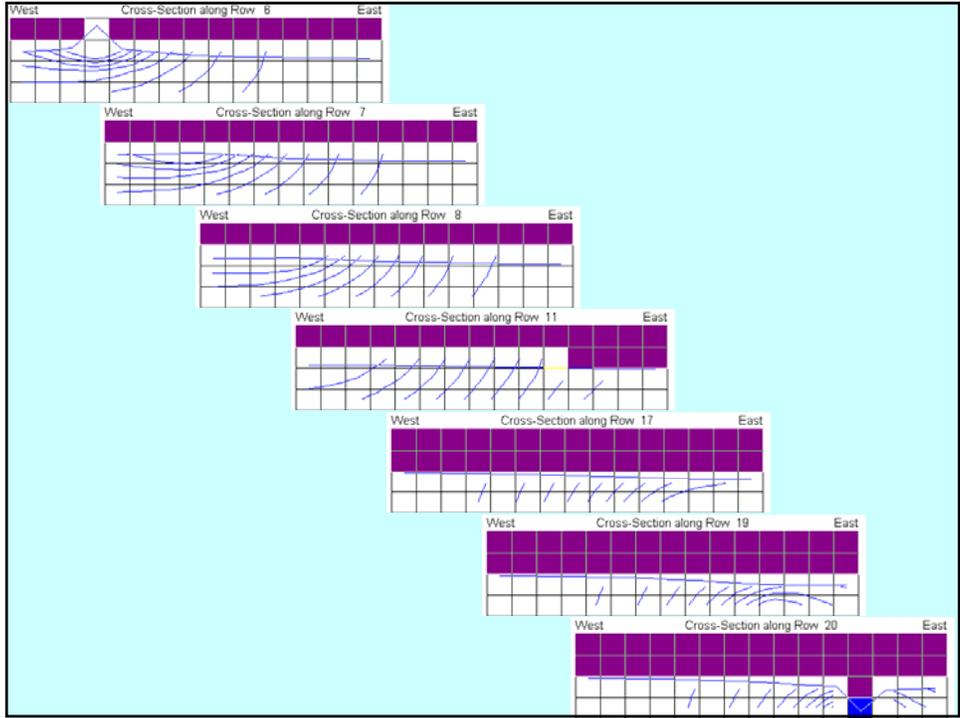


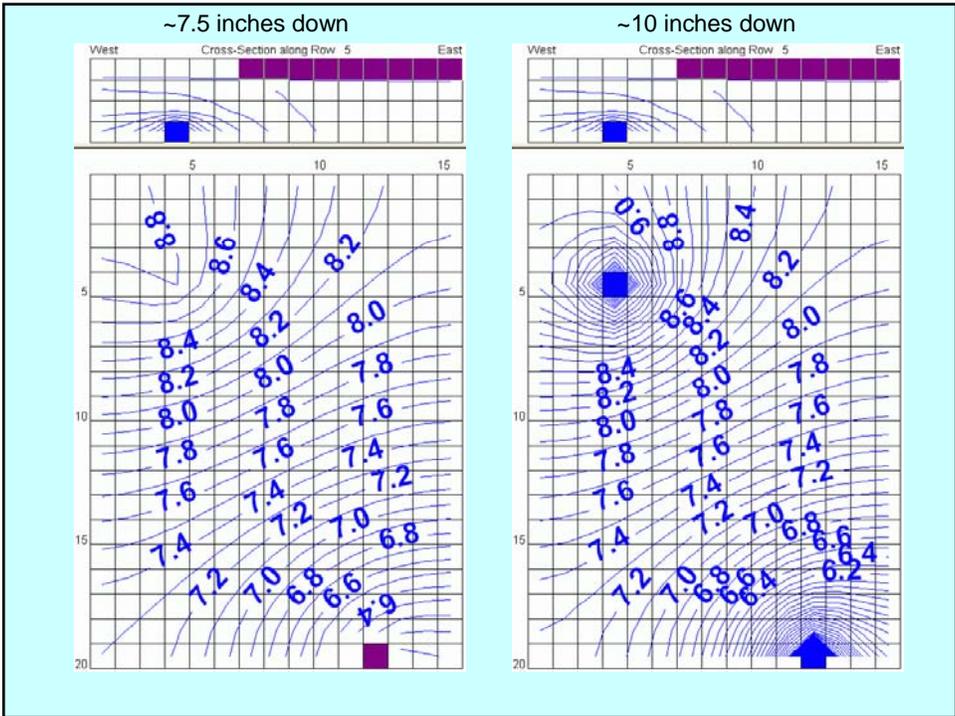
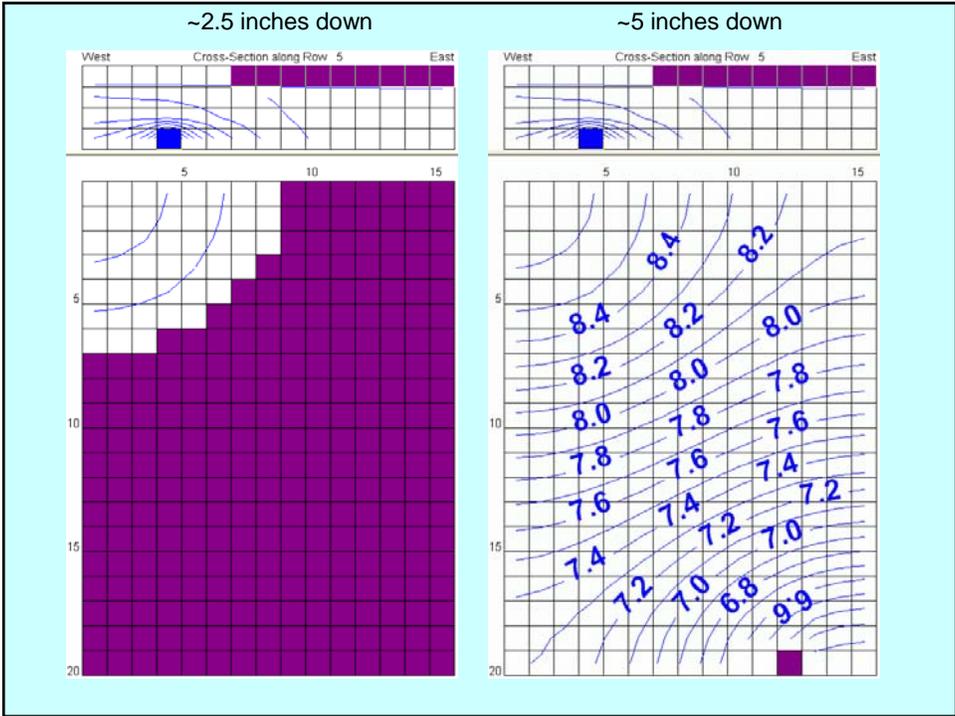
Take the 10x exaggeration figure and shrink to 0.1x

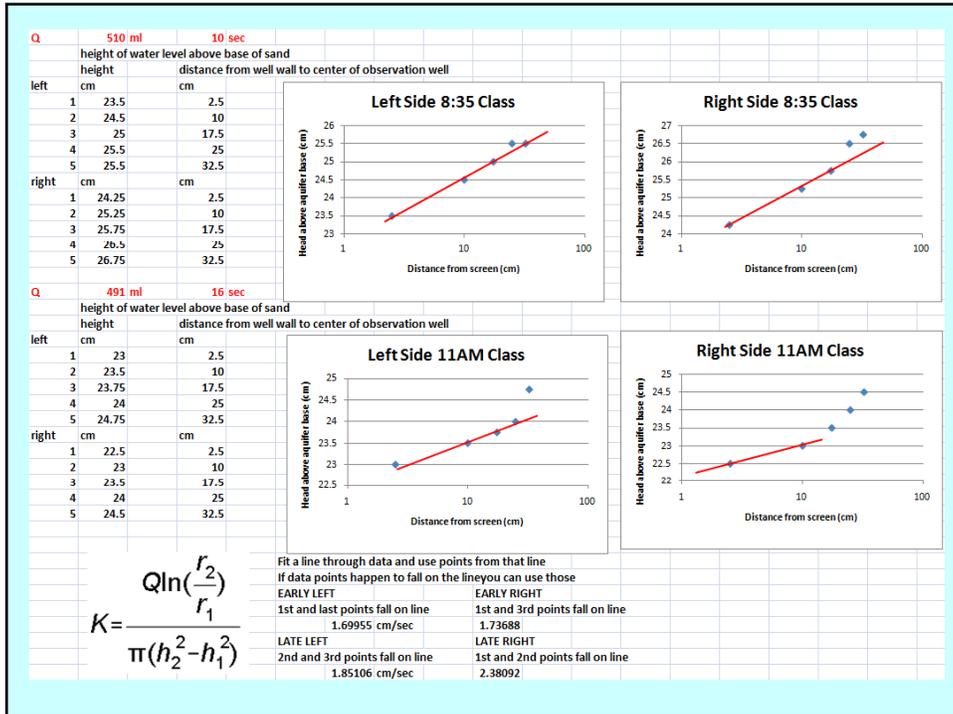
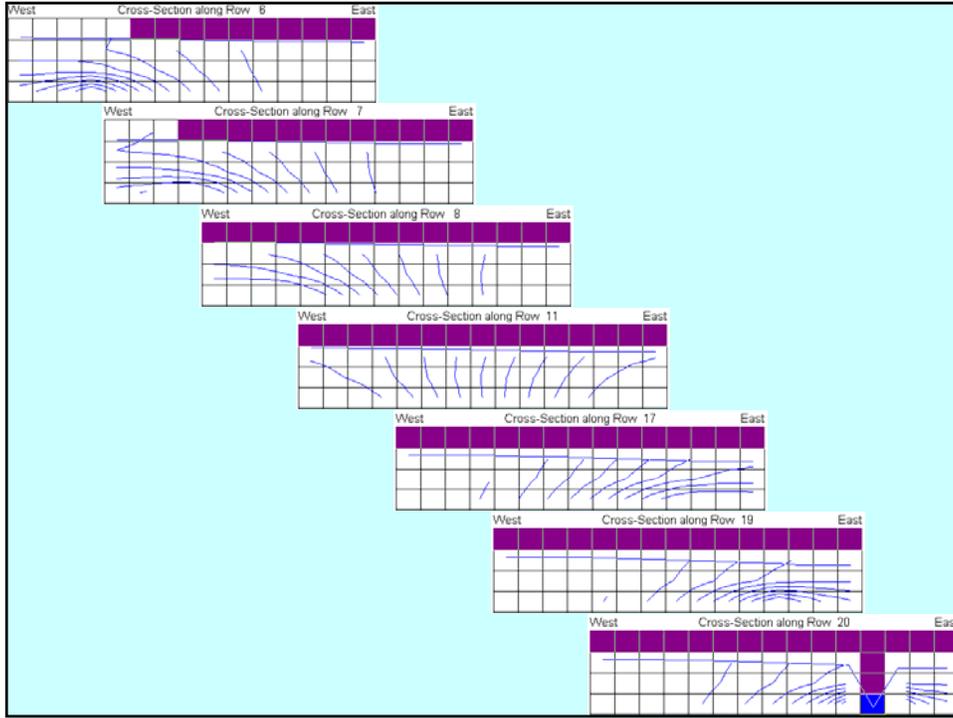












What are K? T?
 Are they different on the left and right?

The Ks do not differ left and right. The affect of the boundaries leads to different K calculations because the equation assumes the aquifer stretches to infinity.

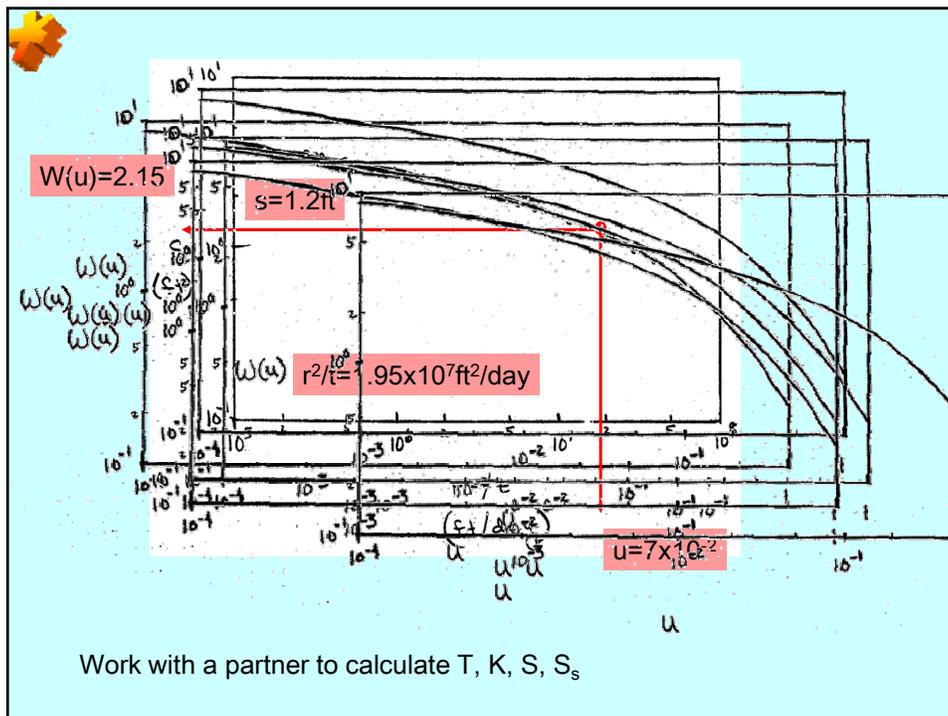
If there was not as much head loss across the screens then

Right side gradient would be steeper due to reservoir boundary
 and K would be underestimated

Left side gradient would be shallower due to no-flow boundary
 and K would be overestimated

More on this in a future lecture

$$K = \frac{Q \ln\left(\frac{r_2}{r_1}\right)}{\pi(h_2^2 - h_1^2)}$$



$$T = \frac{Q}{4\pi s} W(u) = \frac{500 \frac{\text{gal}}{\text{min}} \frac{1 \text{ft}^3}{7.48 \text{gal}} \frac{60(24) \text{min}}{\text{day}} \cdot 2.15}{4\pi \cdot 1.2 \text{ft}} = 13724 \text{ft}^2/\text{day} \approx 1.4 \times 10^4 \frac{\text{ft}^2}{\text{day}}$$

$$K = T/b = 140 \text{ft/day}$$

$$S = \frac{4Tu}{(r^2/t)} = \frac{4(13724 \text{ft}^2/\text{day})(7 \times 10^{-2})}{1.95 \times 10^7 \text{ft}^2/\text{day}} = 2 \times 10^{-4}$$

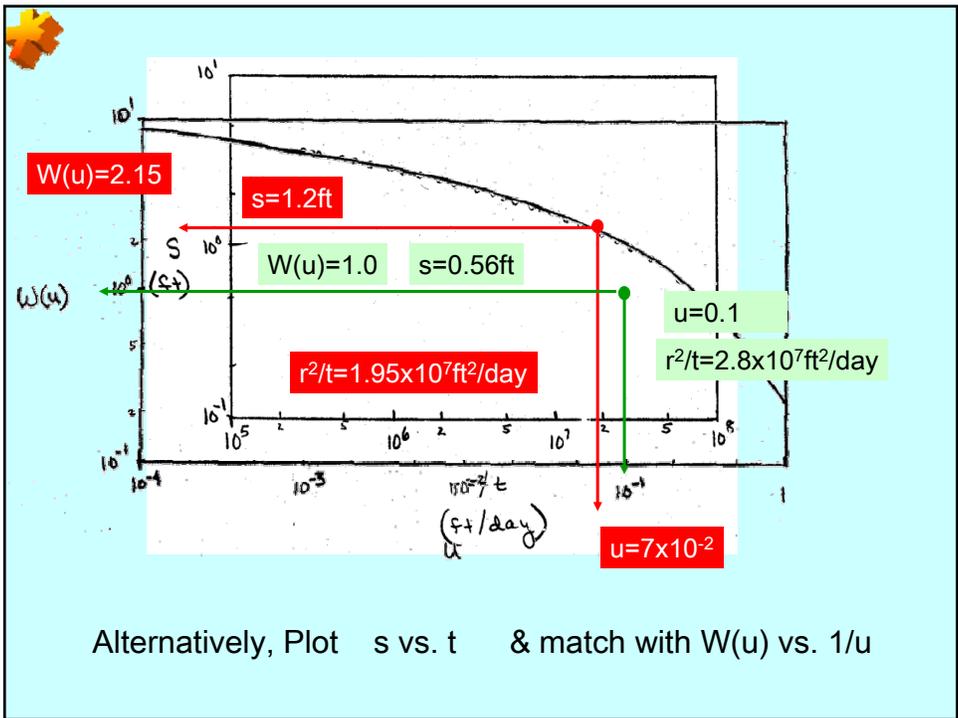
specific storage = $\frac{S}{b} = 2 \times 10^{-6} \text{ft}^{-1}$

Any point can be used. It need not be on the curve. Why?
 (see next slide)

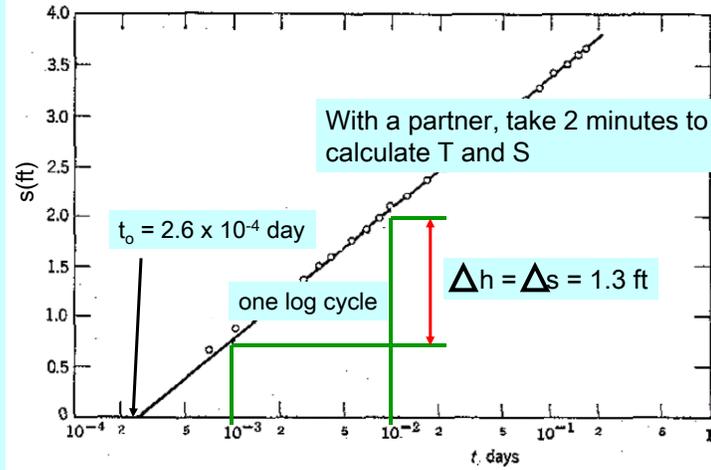
$W(u) = 1$ $s = 0.56$
 $u = 0.1$ $r^2/t = 2.8 \times 10^7$

The curve match identifies the appropriate relative values.

$T = 13678 \text{ft}^2/\text{day}$ approx. $1.4 \times 10^4 \text{ft}^2/\text{day}$
 $S = 1.95 \times 10^{-4}$ approx. 2×10^{-4}



For the Ohio example $Q=500\text{GPM}$, $b=100\text{ft}$, $r=200\text{ft}$
 Plot s vs t



$$T = \frac{2.3Q}{4\pi\Delta h} \quad S = \frac{2.25Tt_0}{r^2}$$



$$T = \frac{2.3Q}{4\pi\Delta h}$$

Δh = drawdown over 1 log cycle of time

$$= \frac{(2.3) 500 \frac{\text{gal}}{\text{min}} \frac{1\text{ft}^3}{7.48\text{gal}} \frac{60(24)\text{min}}{\text{day}}}{4\pi 1.3\text{ft}}$$

$$= 13,552 \text{ ft}^2/\text{day} \sim 1.4 \times 10^4 \text{ ft}^2/\text{day}$$

$$S = \frac{2.25Tt_0}{r^2}$$

t_0 = time intercept for zero drawdown

$$= \frac{2.25 * 13,552 \text{ ft}^2/\text{day} * 2.6 \times 10^{-4} \text{ day}}{(200\text{ft})^2}$$

$$= \sim 1.98 \times 10^{-4} \sim 2 \times 10^{-4}$$

Match:

(there are many possible match points, this is just one)

$$s = 1\text{ft}$$

$$W(u) \sim 0.4$$

$$t = 100\text{s}$$

$$1/u \sim 0.6$$

Calculations:

$$T \sim 1.2 \times 10^{-3} \quad K \sim 1.4 \times 10^{-5}$$

$$\text{rounding } T \sim 1 \times 10^{-3} \quad K \sim 1 \times 10^{-5}$$

$$S \sim 8.3 \times 10^{-7} \quad Ss \sim 9.4 \times 10^{-9}$$

$$\text{rounding } S \sim 1 \times 10^{-6} \quad Ss \sim 1 \times 10^{-8}$$