

PEGN 624 Project  
S2009  
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## Definitions

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### Initialization

#### ■ Data

#### ■ Grid Constants

```
In[1]:= Δx = 100 ; (*ft*)  
In[2]:= Δy = 100; (*ft*)  
In[3]:= Δz = 20; (*ft*)  
In[307]:= Δt = 1; (* day *)  
In[554]:= VR = Δx * Δy * Δz  
Out[554]= 200 000  
In[555]:= VRdt = VR / Δt  
Out[555]= 200 000
```

#### ■ Tolerances

```
In[312]:= εP = 1. * 10 ^ (-3)  
          εSo = εSg = 1. * 10 ^ (-4)  
          εTs = εT = 1. * 10 ^ (-1)  
          εG = 1. * 10 ^ (-2)  
Out[312]= 0.001  
Out[313]= 0.0001  
Out[314]= 0.1  
Out[315]= 0.01
```

#### ■ Rock Properties

```
In[4]:= km = 3000; (*md*)  
In[5]:= φm = 0.3;  
In[6]:= convertk = 0.006328  
Out[6]= 0.006328
```

---

In[7]:= **convertq** = 5.6146

Out[7]= 5.6146

In[11]:= **convertT** = 459.67

Out[11]= 459.67

In[87]:= **convertU** =  $\left(\frac{144}{778.26}\right)$

Out[87]= 0.185028

### ■ Molecular Weight

In[82]:= **MWo** = 250;

In[83]:= **MWg** = **MWw** = 18;

### ■ Thermal Properties

In[304]:= **ρR** = 170 (\* lbm/ft<sup>3</sup> \*)

Out[304]= 170

In[305]:= **CR** = 0.206 (\* btu/(lbm °F) \*)

Out[305]= 0.206

In[306]:= **kT** = 1.6 \* 24 (\* btu/(day ft °F) \*)

Out[306]= 38.4

In[694]:= **TR** = 100;

### ■ Ts

Correlations: T in °F; P in psia

In[198]:= **calcTs**[P\_] := 116 (P) ^ 0.224

In[199]:= **calcTs**[P\_, T\_] := **calcTs**[P]

In[200]:= **calcTs**[100]

Out[200]= 325.43

In[201]:= **calcTs**[600]

Out[201]= 486.143

### ■ Viscosities

Correlations: T in °F

In[202]:= **calcμo**[T\_] := 3.62431 \* 10<sup>-4</sup> Exp[8485.4 / (T + **convertT**)]

In[203]:= **calcμo**[P\_, T\_] := **calcμo**[T]

In[204]:= {calc $\mu$ o[100], calc $\mu$ o[400]}

Out[204]= {1392.36, 7.01363}

In[205]:= calc $\mu$ w[T\_] := 
$$\frac{2.185}{(0.04012 T + 5.1547 * 10^{(-6)} * (T^2) - 1)}$$

In[206]:= calc $\mu$ w[P\_, T\_] := calc $\mu$ w[T]

In[207]:= {calc $\mu$ w[100], calc $\mu$ w[400]}

Out[207]= {0.713226, 0.137657}

In[208]:= calc $\mu$ g[T\_] :=  $8.822 * 10^{(-6)} (T + \text{convert}T)^{1.116}$

In[209]:= calc $\mu$ g[P\_, T\_] := calc $\mu$ g[T]

In[210]:= {calc $\mu$ g[100], calc $\mu$ g[400]}

Out[210]= {0.0102863, 0.0166066}

### ■ Molar Density

Correlations: T in °F; P in psia

In[211]:= calc $\xi$ o[P\_, T\_] :=  $1.683 * (0.1987 - 7.5885 * 10^{(-5)} * (T + \text{convert}T)) * \text{Exp}[10^{(-5)} * (P - 14.7)]$

In[212]:= {calc $\xi$ o[100, 100], calc $\xi$ o[100, 400], calc $\xi$ o[600, 100], calc $\xi$ o[600, 400]}

Out[212]= {0.263159, 0.224811, 0.264478, 0.225938}

In[213]:= calc $\xi$ w[P\_, T\_] :=  $22.14 * (0.202 - 7.725 * 10^{(-5)} * (T + \text{convert}T)) * \text{Exp}[4 * 10^{(-6)} * (P - 118)]$

In[214]:= {calc $\xi$ w[100, 100], calc $\xi$ w[100, 400], calc $\xi$ w[600, 100], calc $\xi$ w[600, 400]}

Out[214]= {3.51481, 3.00176, 3.52185, 3.00777}

May need to use other correlation where  $P > 1000$ .

In[215]:= calc $\xi$ g[P\_] := 
$$\frac{P^{0.9585}}{363.9 * 18}$$

In[216]:= calc $\xi$ g[P\_, T\_] := calc $\xi$ g[P]

In[217]:= {calc $\xi$ g[100], calc $\xi$ g[600]}

Out[217]= {0.0126109, 0.0702431}

### ■ Molar Density Derivatives

In[140]:= calcD $\xi$ oDP[P\_, T\_] :=  $10^{(-5)} * \text{calc}\xi\text{o}[P, T]$

In[141]:= {calcD $\xi$ oDP[100, 100], calcD $\xi$ oDP[100, 400], calcD $\xi$ oDP[600, 100], calcD $\xi$ oDP[600, 400]}

Out[141]= { $2.63159 \times 10^{-6}$ ,  $2.24811 \times 10^{-6}$ ,  $2.64478 \times 10^{-6}$ ,  $2.25938 \times 10^{-6}$ }

In[142]:= D[calc $\xi$ o[P, T], T]

Out[142]=  $-0.000127714 e^{\frac{-14.7 * P}{100000}}$

```

In[143]:= calcDξoDT[P_, T_] := -0.00012771445500000002` e $\frac{-14.7+P}{100000}$ 
In[144]:= {calcDξoDT[100, 100], calcDξoDT[100, 400], calcDξoDT[600, 100], calcDξoDT[600, 400]}
Out[144]= {-0.000127823, -0.000127823, -0.000128464, -0.000128464}

In[145]:= calcDξwDP[P_, T_] := 4 * 10-6 * calcξw[P, T]
In[146]:= {calcDξwDP[100, 100], calcDξwDP[100, 400], calcDξwDP[600, 100], calcDξwDP[600, 400]}
Out[146]= {0.0000140593, 0.000012007, 0.0000140874, 0.0000120311}

In[147]:= D[calcξw[P, T], T]
Out[147]= -0.00171032 e $\frac{-118+P}{250000}$ 

In[148]:= calcDξwDT[P_, T_] := -0.00171031500000000002` e $\frac{-118+P}{250000}$ 
In[149]:= {calcDξwDT[100, 100], calcDξwDT[100, 400], calcDξwDT[600, 100], calcDξwDT[600, 400]}
Out[149]= {-0.00171019, -0.00171019, -0.00171362, -0.00171362}

In[150]:= calcDξgDP[P_] := 0.9585 *  $\frac{P^{(0.9585 - 1)}}{363.9 * 18}$ 
In[151]:= calcDξgDP[P_, T_] := calcDξgDP[P]
In[152]:= {calcDξgDP[100], calcDξgDP[600]}
Out[152]= {0.000120875, 0.000112213}

In[626]:= calcDξgDT[P_, T_] := 0

```

### ■ Specific Gravities

```

In[293]:= convertdensity = 0.4335275 (*psi/ft->g/cm^3*)
Out[293]= 0.433528

In[294]:= baseρw = 62.42796
Out[294]= 62.428

In[295]:= calcγo[P_, T_] :=  $\frac{Mw_o \text{ calc}\xi_o[P, T]}{\text{base}\rho_w}$  * convertdensity
In[296]:= {calcγo[100, 100], calcγo[100, 400], calcγo[600, 100], calcγo[600, 400]}
Out[296]= {0.456872, 0.390298, 0.459163, 0.392254}

In[297]:= calcγw[P_, T_] :=  $\frac{Mw_w \text{ calc}\xi_w[P, T]}{\text{base}\rho_w}$  * convertdensity
In[298]:= {calcγw[100, 100], calcγw[100, 400], calcγw[600, 100], calcγw[600, 400]}
Out[298]= {0.439352, 0.37522, 0.440231, 0.375971}

In[299]:= calcγg[P_, T_] :=  $\frac{Mw_g \text{ calc}\xi_g[P, T]}{\text{base}\rho_w}$  * convertdensity

```

```
In[300]:= {calcγg[100, 100], calcγg[100, 400], calcγg[600, 100], calcγg[600, 400]}
Out[300]= {0.00157636, 0.00157636, 0.00878038, 0.00878038}
```

### ■ Heat Capacities

Correlations: T in °F; P in psia

```
In[153]:= calcCpo[T_] := 57.88 + 6.03 * 10^(-2) (T + convertT)
In[154]:= calcCpo[P_, T_] := calcCpo[T]
In[155]:= {calcCpo[100], calcCpo[400]}
Out[155]= {91.6281, 109.718}

In[156]:= calcCpw[T_] := 41.809 - 7.8289 * 10^(-2) (T + convertT) + 6.2788 * 10^(-5) (T + convertT)^2
In[157]:= calcCpw[P_, T_] := calcCpw[T]
In[158]:= {calcCpw[100], calcCpw[400]}
Out[158]= {17.6601, 20.9087}

In[159]:= calcCpg[T_] := 7.136 + 1.4667 * 10^(-3) (T + convertT) + 2.55 * 10^(-8) (T + convertT)^2
In[160]:= calcCpg[P_, T_] := calcCpg[T]
In[161]:= {calcCpg[100], calcCpg[400]}
Out[161]= {7.96486, 8.41572}
```

### ■ Enthalpies

Correlations: T in °F; P in psia

```
In[162]:= Integrate[calcCpo[To], {To, 32, 77}]
Out[162]= 3999.8

In[163]:= Integrate[calcCpo[To], {To, 77, T}]
Out[163]= -6769.81 + 85.5981 T + 0.03015 T^2

In[164]:= calcHo[T_] :=
  3999.8002950000005` + -6769.813127000001` + 85.59810100000001` T + 0.030150000000000003` T^2
In[165]:= calcHo[P_, T_] := calcHo[T]

In[166]:= Integrate[calcCpw[To], {To, 32, T}]
Out[166]= -600.997 + 19.0888 T - 0.0102827 T^2 + 0.0000209293 T^3

In[167]:= calcHwless[T_] := -600.9972648597292` +
  19.088780570813203` T - 0.010282740039999995` T^2 + 0.0000209293333333333336` T^3
In[168]:= calcHwless[P_, T_] := calcHwless[T]

In[169]:= Integrate[calcCpw[To], {To, 32, calcTs[P]}]
Out[169]= -600.997 + 2214.3 P^0.224 - 138.365 P^0.448 + 32.6685 P^0.672
```

```
In[170]:= calcHwmore [P_] := -600.9972648597292` +
      2214.2985462143315` P0.224` - 138.36454997823992` P0.448` + 32.66851268266667` P0.672`
```

```
In[171]:= calcHwmore [P_, T_] := calcHwmore [P]
```

```
In[172]:= calcHwmore [P_, T_] := calcHwmore [P] + 1318  $\left(\left(\frac{T}{116}\right)^{4.464}\right)^{-0.08774}$ 
```

### Internal Energies

```
In[190]:= calcUo [P_, T_] := calcHo [T] - convertU  $\frac{P}{Mw \text{ calc}\xi o [P, T]}$ 
```

```
In[191]:= {calcUo [100, 100], calcUo [100, 400], calcUo [600, 100], calcUo [600, 400]}
```

```
Out[191]= {6091.02, 36292.9, 6089.62, 36291.3}
```

```
In[192]:= calcUwless [P_, T_] := calcHwless [T] - convertU  $\frac{P}{Mw \text{ calc}\xi w [P, T]}$ 
```

```
In[193]:= {calcUwless [100, 100], calcUwless [100, 400], calcUwless [600, 100], calcUwless [600, 400]}
```

```
Out[193]= {1225.69, 6728.41, 1224.23, 6726.7}
```

```
In[194]:= calcUwmore [P_, T_] := calcHwmore [P] - convertU  $\frac{P}{Mw \text{ calc}\xi w [P, T]}$ 
```

```
In[195]:= {calcUwmore [100, 500], calcUwmore [100, 1000], calcUwmore [600, 500], calcUwmore [600, 1000]}
```

```
Out[195]= {5243.04, 5242.88, 8651.16, 8650.21}
```

```
In[196]:= calcUgmore [P_, T_] := calcHgmore [P, T] - convertU  $\frac{P}{Mw \text{ calc}\xi g [P]}$ 
```

```
In[197]:= {calcUgmore [100, 500], calcUgmore [100, 1000], calcUgmore [600, 500], calcUgmore [600, 1000]}
```

```
Out[197]= {5905.58, 5728.77, 9309.22, 9132.4}
```

### Internal Energies Derivatives

```
In[259]:= D[calcUo [P, T], T]
```

```
Out[259]= 85.5981 + 0.0603 T -  $\frac{3.3371 \times 10^{-8} e^{\frac{14.7-P}{100000} P}}{(0.1987 - 0.000075885 (459.67 + T))^2}$ 
```

```
In[260]:= calcDUoDT [P_, T_] := 85.59810100000001` +
```

```
0.060300000000000006` T -  $\frac{3.337102883149041 \times 10^{-8} e^{\frac{14.7-P}{100000} P}}{(0.1987 - 0.00007588500000000001 (459.67 + T))^2}$ 
```

```
In[261]:= {calcDUoDT [100, 100], calcDUoDT [100, 400], calcDUoDT [100, 1000],
      calcDUoDT [600, 100], calcDUoDT [600, 400], calcDUoDT [600, 1000]}
```

```
Out[261]= {91.628, 109.718, 145.898, 91.6273, 109.717, 145.896}
```

In[262]:= **D[calcUo[P, T], P]**

$$\text{Out[262]} = -\frac{0.000439758 e^{\frac{14.7-P}{100000}}}{0.1987 - 0.000075885 (459.67 + T)} + \frac{4.39758 \times 10^{-9} e^{\frac{14.7-P}{100000}} P}{0.1987 - 0.000075885 (459.67 + T)}$$

$$\text{In[263]} := \text{calcDUoDP}[P_, T_] := -\frac{0.0004397579077747962 e^{\frac{14.7-P}{100000}}}{0.1987 - 0.00007588500000000001 (459.67 + T)} + \frac{4.397579077747962 e^{\frac{14.7-P}{100000}} P}{0.1987 - 0.00007588500000000001 (459.67 + T)}$$

In[264]:= {calcDUoDP[100, 100], calcDUoDP[100, 400], calcDUoDP[100, 1000], calcDUoDP[600, 100], calcDUoDP[600, 400], calcDUoDP[600, 1000]}

Out[264]= {-0.00280961, -0.00328886, -0.0049918, -0.0027816, -0.00325607, -0.00494204}

In[265]:= **D[calcUwless[P, T], T]**

$$\text{Out[265]} = 19.0888 - 0.0205655 T + 0.000062788 T^2 - \frac{3.58663 \times 10^{-8} e^{\frac{118-P}{250000}} P}{(0.202 - 0.00007725 (459.67 + T))^2}$$

$$\text{In[266]} := \text{calcDUwlessDT}[P_, T_] := 85.598101000000001 + 0.060300000000000006 T - \frac{3.337102883149041 e^{\frac{14.7-P}{100000}} P}{(0.1987 - 0.00007588500000000001 (459.67 + T))^2}$$

In[267]:= {calcDUwlessDT[100, 100], calcDUwlessDT[100, 400], calcDUwlessDT[600, 100], calcDUwlessDT[600, 400]}

Out[267]= {91.628, 109.718, 91.6273, 109.717}

In[268]:= **D[calcUwless[P, T], P]**

$$\text{Out[268]} = -\frac{0.000464288 e^{\frac{118-P}{250000}}}{0.202 - 0.00007725 (459.67 + T)} + \frac{1.85715 \times 10^{-9} e^{\frac{118-P}{250000}} P}{0.202 - 0.00007725 (459.67 + T)}$$

In[269]:= **calcDUwlessDP[P\_, T\_] :=**

$$-\frac{0.00046428821563847613 e^{\frac{118-P}{250000}}}{0.202 - 0.00007725000000000001 (459.67 + T)} + \frac{1.8571528625539045 e^{\frac{118-P}{250000}} P}{0.202 - 0.00007725000000000001 (459.67 + T)}$$

In[270]:= {calcDUwlessDP[100, 100], calcDUwlessDP[100, 400], calcDUwlessDP[600, 100], calcDUwlessDP[600, 400]}

Out[270]= {-0.00292341, -0.00342307, -0.00291173, -0.0034094}

In[271]:= **D[calcUwmore[P, T], T]**

$$\text{Out[271]} = -\frac{3.58663 \times 10^{-8} e^{\frac{118-P}{250000}} P}{(0.202 - 0.00007725 (459.67 + T))^2}$$

$$\text{In[272]} := \text{calcDUwmoreDT}[P_, T_] := -\frac{3.586626465807229 e^{\frac{118-P}{250000}} P}{(0.202 - 0.00007725000000000001 (459.67 + T))^2}$$

In[273]:= {calcDUwmoreDT[100, 500], calcDUwmoreDT[100, 1000],  
calcDUwmoreDT[600, 500], calcDUwmoreDT[600, 1000]}

Out[273]:= {-0.000219387, -0.000450395, -0.00131369, -0.00269697}

In[274]:= D[calcUwmore[P, T], P]

$$\text{Out[274]} = \frac{496.003}{p^{0.776}} - \frac{61.9873}{p^{0.552}} + \frac{21.9532}{p^{0.328}} - \frac{0.000464288 e^{\frac{118-P}{250000}}}{0.202 - 0.00007725 (459.67 + T)} + \frac{1.85715 \times 10^{-9} e^{\frac{118-P}{250000}} P}{0.202 - 0.00007725 (459.67 + T)}$$

$$\text{In[275]} := \text{calcDUwmoreDP}[P_, T_] := \frac{496.0028743520103^{\sim}}{p^{0.776^{\sim}}} - \frac{61.98731839025149^{\sim}}{p^{0.552^{\sim}}} + \frac{21.953240522752004^{\sim}}{p^{0.32799999999999996^{\sim}}} - \frac{0.00046428821563847613^{\sim} e^{\frac{118-P}{250000}}}{0.202^{\sim} - 0.00007725000000000001^{\sim} (459.67^{\sim} + T)} + \frac{1.8571528625539045^{\sim} * 10^{-9} e^{\frac{118-P}{250000}} P}{0.202^{\sim} - 0.00007725000000000001^{\sim} (459.67^{\sim} + T)}$$

In[276]:= {calcDUwmoreDP[100, 500], calcDUwmoreDP[100, 1000],  
calcDUwmoreDP[600, 500], calcDUwmoreDP[600, 1000]}

Out[276]:= {13.88, 13.8784, 4.33952, 4.33796}

In[277]:= D[calcUgmore[P, T], T]

$$\text{Out[277]} = -\frac{3322.2 T^{3.464}}{(T^{4.464})^{1.08774}}$$

$$\text{In[278]} := \text{calcDUgmoreDT}[P_, T_] := -\frac{3322.203982900616^{\sim} T^{3.4640000000000004^{\sim}}}{(T^{4.464^{\sim}})^{1.08774^{\sim}}}$$

In[279]:= {calcDUgmoreDT[100, 500], calcDUgmoreDT[100, 1000],  
calcDUgmoreDT[600, 500], calcDUgmoreDT[600, 1000]}

Out[279]:= {-0.582569, -0.22203, -0.582569, -0.22203}

In[280]:= D[calcUgmore[P, T], P]

$$\text{Out[280]} = -\frac{2.79427}{p^{0.9585}} + \frac{496.003}{p^{0.776}} - \frac{61.9873}{p^{0.552}} + \frac{21.9532}{p^{0.328}}$$

$$\text{In[281]} := \text{calcDUgmoreDP}[P_, T_] := -\frac{2.7942672114717433^{\sim}}{p^{0.9585^{\sim}}} + \frac{496.0028743520103^{\sim}}{p^{0.776^{\sim}}} - \frac{61.98731839025149^{\sim}}{p^{0.552^{\sim}}} + \frac{21.953240522752004^{\sim}}{p^{0.32799999999999996^{\sim}}}$$

In[282]:= {calcDUgmoreDP[100, 500], calcDUgmoreDP[100, 1000],  
calcDUgmoreDP[600, 500], calcDUgmoreDP[600, 1000]}

Out[282]:= {13.8498, 13.8498, 4.33706, 4.33706}

■ Compressibilities

In[301]:=  $c\phi = 10 * 10^{(-6)}; (* psi^{-1} *)$

■ Source Terms

In[568]:=  $flowsource = 35000. / 18$

Out[568]= 1944.44



```
In[572]:= heatsource = 1000. * flowsource
```

```
Out[572]= 1.94444 × 106
```

## ■ Capillary Pressure, Rel Perm

### ■ Rel Perm

#### Saturations

```
In[484]:= Swrm = 0.20;
           Sowrm = 0.30;
           Sogrm = 0.20;
           Sgcm = 0.05;
```

#### Rel Perm

```
In[488]:= krwmstar = 0.2;
           nwm = 3.0;
```

```
In[490]:= krowmstar = 0.6;
           nowm = 4.0;
```

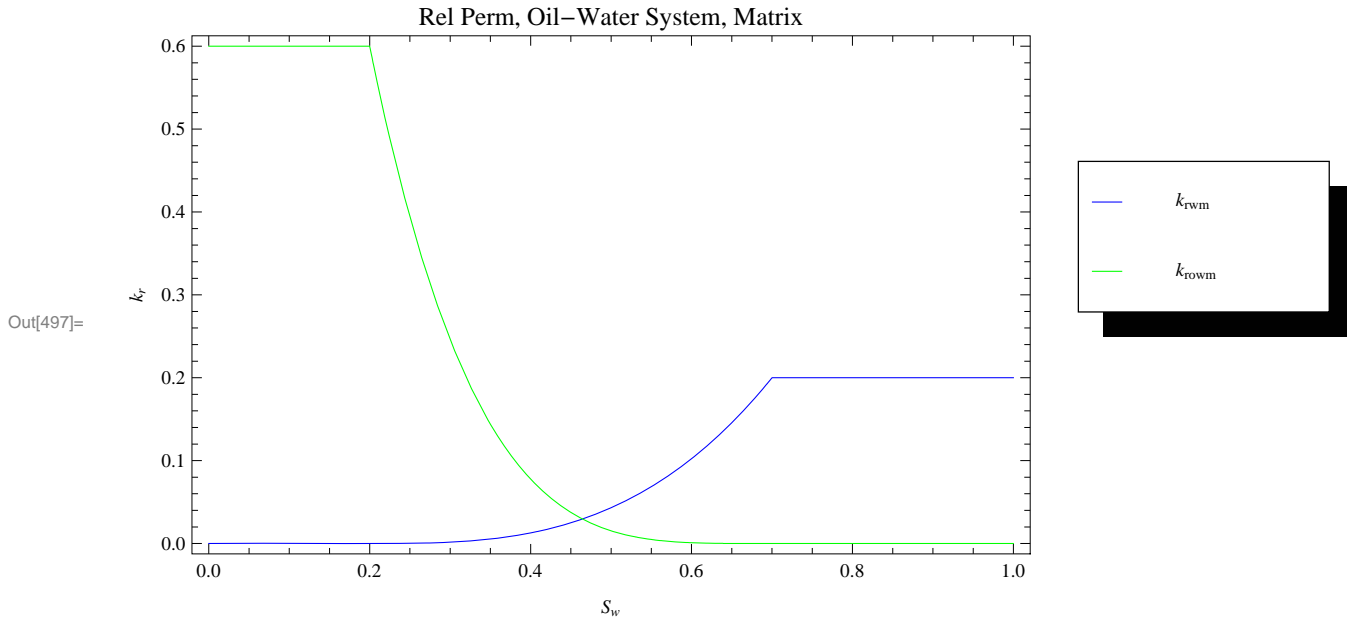
```
In[492]:= krgmstar = 0.5;
           ngm = 3.0;
```

```
In[494]:= computekrwm[Sw_] :=
           Which[Sw ≤ Swrm, 0,
                Sw ≥ (1 - Sowrm), krwmstar,
                True,
                krwmstar *  $\left(\frac{(Sw - Swrm)}{(1 - Swrm - Sowrm)}\right)^{nwm}$ 
           ]
```

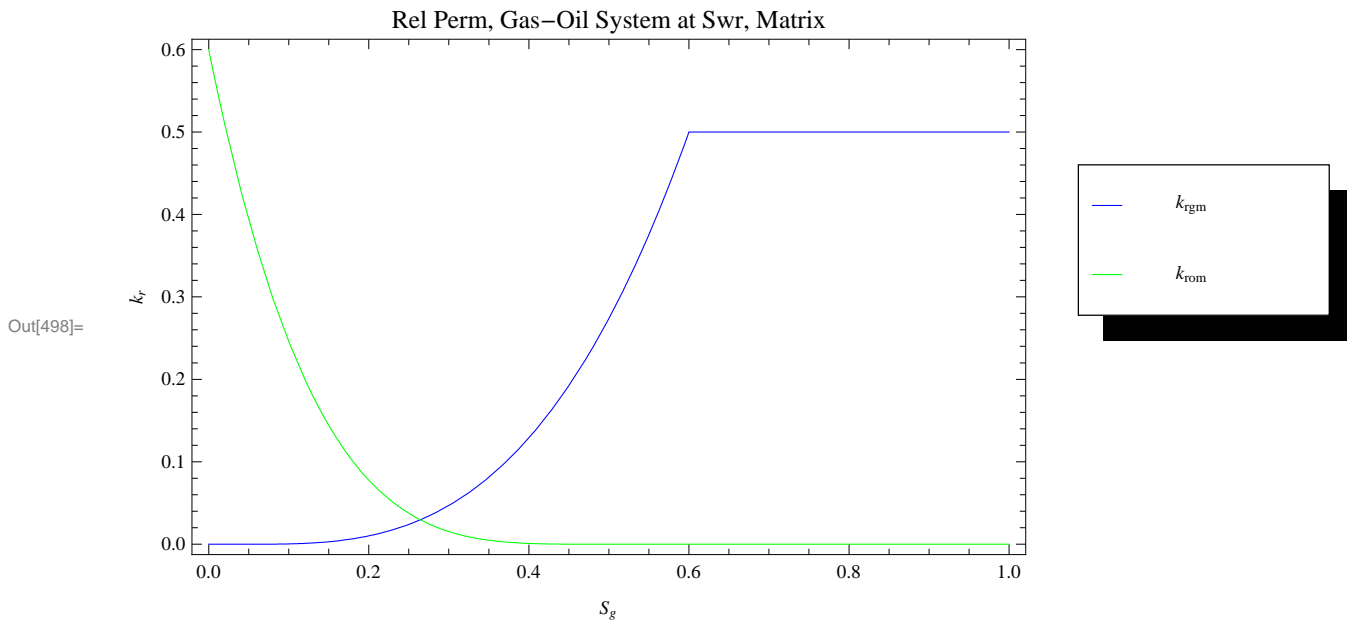
```
In[495]:= computekrowm[So_] :=
           Which[So ≤ Sowrm, 0,
                So ≥ (1 - Swrm), krowmstar,
                True,
                krowmstar *  $\left(\frac{(So - Sowrm)}{(1 - Swrm - Sowrm)}\right)^{nowm}$ 
           ]
```

```
In[496]:= computekrgm[Sg_] :=
           Which[Sg ≤ Sgcm, 0,
                Sg ≥ (1 - Swrm - Sogrm), krgmstar,
                True,
                krgmstar *  $\left(\frac{(Sg - Sgcm)}{(1 - Swrm - Sogrm - Sgcm)}\right)^{ngm}$ 
           ]
```

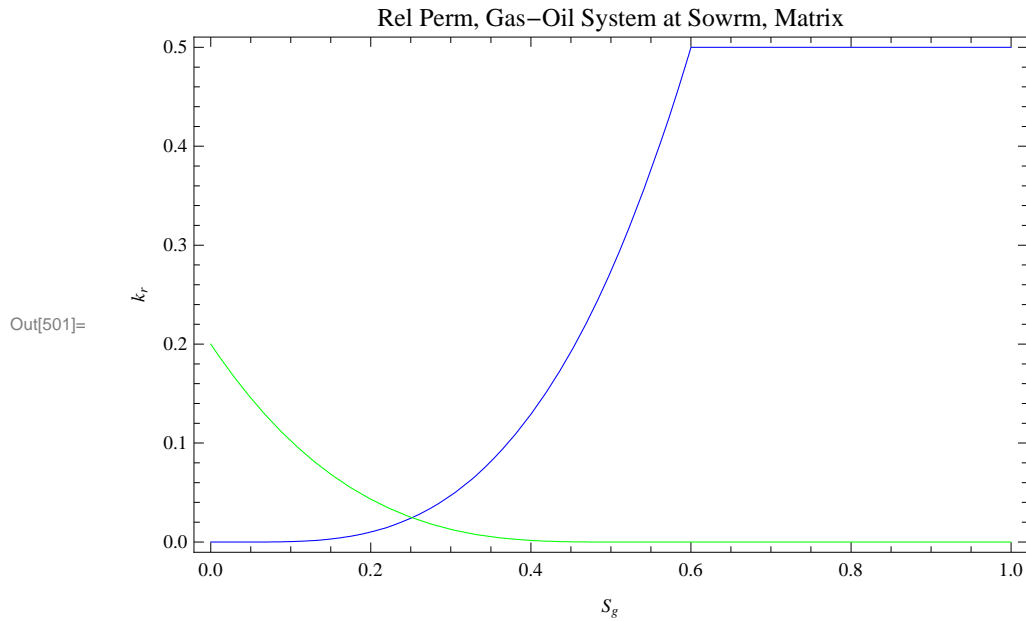
```
In[497]:= Plot[{computekrwm[Sw], computekrowm[1 - Sw]}, {Sw, 0, 1}, Frame -> True,
FrameLabel -> {"Sw", "kr"}, PlotLabel -> "Rel Perm, Oil-Water System, Matrix",
PlotStyle -> {Blue, Green}, ImageSize -> 600, PlotLegend -> {"krwm", "krowm"},
LegendPosition -> {.9, 0}, LegendSize -> {.5, .3}]
```



```
In[498]:= Plot[{computekrgm[Sg], computekrom[1 - Sg - Swrm]}, {Sg, 0, 1}, Frame -> True,
FrameLabel -> {"Sg", "kr"}, PlotLabel -> "Rel Perm, Gas-Oil System at Swr, Matrix",
PlotStyle -> {Blue, Green}, ImageSize -> 600, PlotLegend -> {"krgm", "krom"},
LegendPosition -> {.9, 0}, LegendSize -> {.5, .3}]
```



```
In[501]:= Plot[{computekrgm[Sg], computekrwm[1 - Sg - Sowrm]}, {Sg, 0, 1}, Frame → True,
  FrameLabel → {"Sg", "kr"}, PlotLabel → "Rel Perm, Gas-Oil System at Sowrm, Matrix",
  PlotStyle → {Blue, Green}, ImageSize → 600, PlotLegend → {"krgm", "krwm"},
  LegendPosition → {.9, 0}, LegendSize → {.5, .3}]
```



## ■ Capillary Pressure

### Capillary Pressure

```
In[507]:= Pcowstar = 5;
  Pcogstar = 10;
  Pcogentry = 3;
  ncw = 1.76;
  ncg = 1.20;
```

```
In[512]:= Pcogm1[Sg_] := Pcogentry + Pcogstar *  $\left( \frac{(Sg - Sgcm)}{(1 - Swrm - Sogrm - Sgcm)} \right)^{ncg}$ 
```

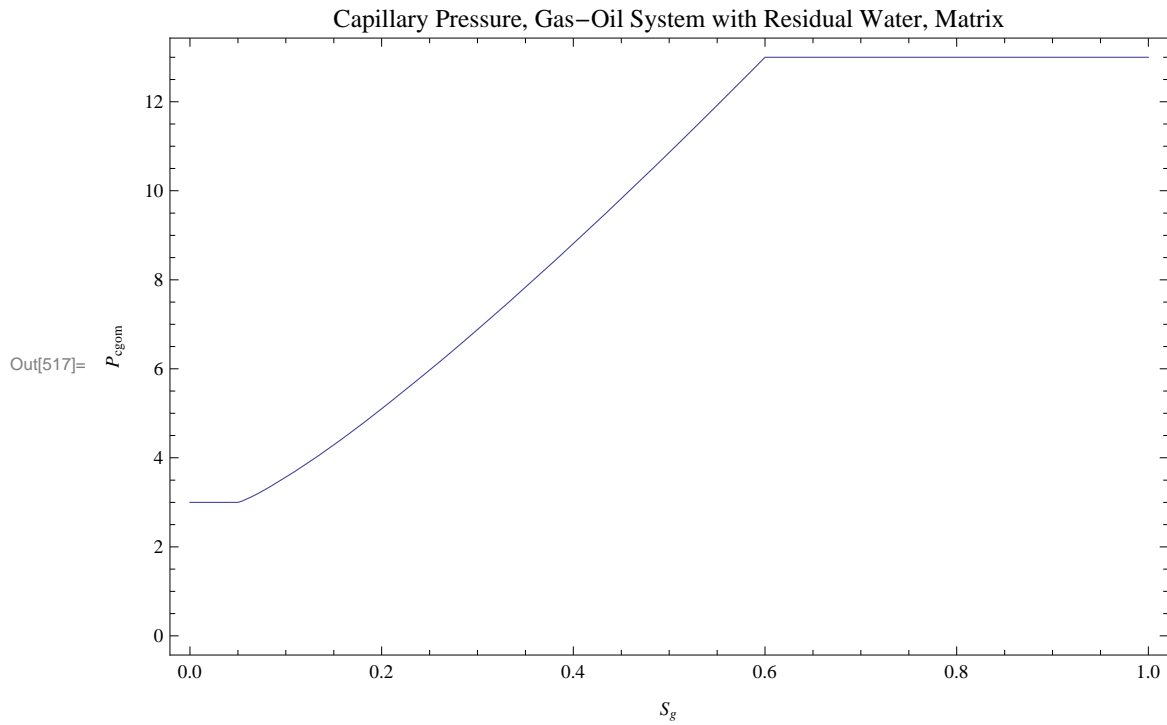
```
In[513]:= Pcowm1[Sw_] := Pcowstar *  $\left( \frac{(1 - Sowrm - Sw)}{(1 - Sowrm - Swrm)} \right)^{ncw}$ 
```

```
In[516]:= computePcogm[Sg_] :=
  Module[{},
    Which[Sg ≤ Sgcm, Pcogentry,
      Sg ≥ (1 - Swrm - Sogrm), Pcogentry + Pcogstar,
      True, Pcogm1[Sg]
    ]
  ]
```

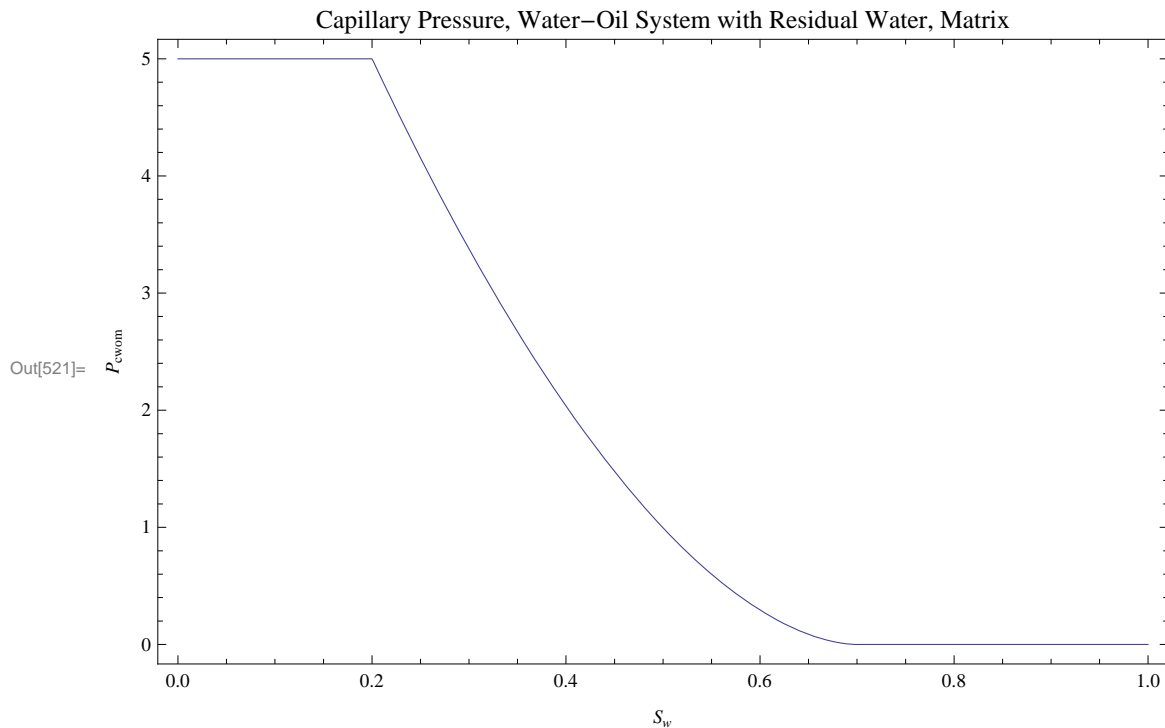
```
In[520]:= computePcwm[Sw_] :=
```

```
Module[{},  
  Which[Sw ≤ Swrm, Pcowstar,  
    Sw ≥ (1 - Swrm), 0,  
    True, Pcowml[Sw]  
  ]]
```

```
In[517]:= Plot[computePcogm[Sg], {Sg, 0, 1}, Frame → True, FrameLabel → {"Sg", "Pcogm"},  
  PlotLabel → "Capillary Pressure, Gas-Oil System with Residual Water, Matrix",  
  ImageSize → 500, PlotRange → All, AxesOrigin → {0, 0}]
```



```
In[521]:= Plot[computePcowm[Sw], {Sw, 0, 1}, Frame → True, FrameLabel → {"Sw", "Pcwom"},
  PlotLabel → "Capillary Pressure, Water-Oil System with Residual Water, Matrix",
  ImageSize → 500, PlotRange → All, AxesOrigin → {0, 0}]
```



## ■ Transmissibilities & Fractional Flows

### ■ Transmissibilities

use upstream only here since  $k$ ,  $\Delta x$  are constant

```
In[536]:= calcTw[P_, T_, So_, Sg_, Sw_] :=
  convertk * km *  $\frac{\text{computekrwm}[Sw]}{\text{calc}\mu_w[P, T]} \frac{(\Delta y \Delta z)}{\Delta x}$ 
```

```
In[537]:= calcTo[P_, T_, So_, Sg_, Sw_] :=
  convertk * km *  $\frac{\text{computekrowm}[So]}{\text{calc}\mu_o[P, T]} \frac{(\Delta y \Delta z)}{\Delta x}$ 
```

```
In[538]:= calcTg[P_, T_, So_, Sg_, Sw_] :=
  convertk * km *  $\frac{\text{computekrgm}[Sg]}{\text{calc}\mu_g[P, T]} \frac{(\Delta y \Delta z)}{\Delta x}$ 
```

```
In[539]:= a1 = {500, 100, 0.8, 0, 0.2}
```

```
Out[539]= {500, 100, 0.8, 0, 0.2}
```

```
In[540]:= {calcTw@@a1, calcTo@@a1, calcTg@@a1}
```

```
Out[540]= {0, 0.163612, 0}
```

```
In[541]:= a2 = {500, 500, 0.7, 0.1, 0.2}
```

```
Out[541]= {500, 500, 0.7, 0.1, 0.2}
```

```
In[542]:= {calcTw@@a2, calcTo@@a2, calcTg@@a2}
```

```
Out[542]= {0, 37.2111, 7.59617}
```

### ■ Thermal Transmissibility

```
In[614]:= TE = kT  $\frac{(\Delta y \Delta z)}{\Delta x}$ 
```

```
Out[614]= 768.
```

### ■ Thermal Boundaries

```
In[695]:= calcqb[T_] := -kT * Δx * Δy *  $\frac{(T - TR)}{\text{Sqrt}\left[\text{Pi} \left(\frac{kT}{\rho R + CR}\right) \Delta t\right]}$ 
```

```
In[614]:= TE = kT  $\frac{(\Delta y \Delta z)}{\Delta x}$ 
```

```
Out[614]= 768.
```

### ■ Fractional Flow

use upstream only here since k, Δx are constant

```
In[588]:= calcλw[P_, T_, So_, Sg_, Sw_] :=  $\frac{\text{computekrwm}[Sw]}{\text{calc}\mu w[P, T]}$ 
```

```
In[589]:= calcλo[P_, T_, So_, Sg_, Sw_] :=  $\frac{\text{computekrowm}[So]}{\text{calc}\mu o[P, T]}$ 
```

```
In[590]:= calcλg[P_, T_, So_, Sg_, Sw_] :=  $\frac{\text{computekrgm}[Sg]}{\text{calc}\mu g[P, T]}$ 
```

```
In[591]:= calcλtot[P_, T_, So_, Sg_, Sw_] :=  $\text{calc}\lambda w[P, T, So, Sg, Sw] + \text{calc}\lambda o[P, T, So, Sg, Sw] + \text{calc}\lambda g[P, T, So, Sg, Sw]$ 
```

```
In[592]:= calcffw[P_, T_, So_, Sg_, Sw_] :=  $\text{calc}\lambda w[P, T, So, Sg, Sw] / \text{calc}\lambda \text{tot}[P, T, So, Sg, Sw]$ 
```

```
In[593]:= calcffo[P_, T_, So_, Sg_, Sw_] :=  $\text{calc}\lambda o[P, T, So, Sg, Sw] / \text{calc}\lambda \text{tot}[P, T, So, Sg, Sw]$ 
```

```
In[594]:= calcffg[P_, T_, So_, Sg_, Sw_] :=  $\text{calc}\lambda g[P, T, So, Sg, Sw] / \text{calc}\lambda \text{tot}[P, T, So, Sg, Sw]$ 
```

```
In[595]:= a1 = {500, 100, 0.8, 0, 0.2}
```

```
Out[595]= {500, 100, 0.8, 0, 0.2}
```

In[596]:= {calcffw@@a1, calcffo@@a1, calcffg@@a1}

Out[596]= {0, 1., 0}

In[597]:= a2 = {500, 500, 0.7, 0.1, 0.2}

Out[597]= {500, 500, 0.7, 0.1, 0.2}

In[598]:= {calcffw@@a2, calcffo@@a2, calcffg@@a2}

Out[598]= {0, 0.83047, 0.16953}

### ■ Thermodynamic Constraints

In[698]:= calcG[P\_, T\_, So\_, Sg\_, Sw\_] :=

$$\left(\frac{T}{116}\right)^{4.464} * \left(\frac{Sw}{Sw + \epsilon G}\right) - P$$

In[700]:= calcDGDP[P\_, T\_, So\_, Sg\_, Sw\_] :=

$$-1$$

In[705]:= calcDGDT[P\_, T\_, So\_, Sg\_, Sw\_] :=

$$\frac{4.464}{116} \left(\frac{T}{116}\right)^{3.464} * \left(\frac{Sw}{Sw + \epsilon G}\right)$$

In[715]:= calcDGDSO[P\_, T\_, So\_, Sg\_, Sw\_] :=

$$\left(\frac{T}{116}\right)^{4.464} * \left(\frac{-\epsilon G}{(Sw + \epsilon G)^2}\right)$$

### ■ At T=100F, P=500

#### ■ Conditions

In[551]:= a1 = {P1 = 500 (\*P\*), T1 = 100 (\*T\*), So1 = 0.8 (\*So\*), Sg1 = 0 (\*Sg\*), Sw1 = 0.2 (\*Sw\*)}

Out[551]= {500, 100, 0.8, 0, 0.2}

In[544]:= a11 = Take[a1, 2]

Out[544]= {500, 100}

In[559]:= T1

Out[559]= 100

In[731]:= Ts1 = calcTs[P1, T1]

Out[731]= 466.689

Thus T1 < Ts

#### ■ Water Equation

Term 1,9,11 ( $\delta P$ )

In[631]:= **W1 = (calcTw@@a1) \* (calcξw@@a11)**

Out[631]= 0

In[632]:= **W9 = -W1**

Out[632]= 0

In[633]:= **W11 = W1**

Out[633]= 0

**Term 2,10,12 ( $\delta P$ )**

In[634]:= **W2 = (calcTg@@a1) \* (calcξg@@a11)**

Out[634]= 0

In[635]:= **W10 = -W2**

Out[635]= 0

In[636]:= **W12 = -W2**

Out[636]= 0

**Term 3 ( $\delta P$ )**

In[637]:= **W3 = -VRdt \* φm \* cφ \* Sw1 \* calcξw[P1, T1] + VRdt \* φm \* Sw1 \* calcDξwDP[P1, T1]**

Out[637]= -0.253472

**Term 4 ( $\delta T$ )**

In[638]:= **W4 = -VRdt \* φm \* Sw1 \* calcDξwDT[P1, T1]**

Out[638]= 20.5552

**Term 5 ( $\delta S_0$ )**

In[639]:= **W5 = VRdt \* φm \* calcξw[P1, T1]**

Out[639]= 211.227.

In[640]:= **W6 = 0**

Out[640]= 0

**Term 7 ( $\ell$ )**

In[641]:= **W7 = VRdt \* (φm \* Sw1 \* calcξw[P1, T1])**

Out[641]= 42.245.3

**Term 8 (n)**

In[642]:= **W8 = -VRdt \* (φm \* Sw1 \* calcξw[P1, T1])**

Out[642]= -42.245.3

**Term 13, 14 : 0 since  $\Delta D = 0$**



In[643]:=  $W13 = W14 = 0$

Out[643]= 0

Term 15, cell 1 injection

$W15a = -\text{flowsource}$

Out[647]= 1944.44

Term 15, cell N production

In[648]:=  $W15c =$   
 $-(-\text{flowsource} * (\text{calcffw}@@a1) * (\text{calc\xi w}@@a11) - \text{flowsource} * (\text{calcffg}@@a1) * (\text{calc\xi g}@@a11))$

Out[648]= 0

### ■ Oil Equation

Term 1,7 ( $\delta P$ )

In[658]:=  $O1 = (\text{calcTo}@@a1) * (\text{calc\xi o}@@a11)$

Out[658]= 0.0432286

In[659]:=  $O7 = -O1$

Out[659]= -0.0432286

Term 2 ( $\delta P$ )

In[660]:=  $O2 = -VRdt * \phi m * S o1 * (c\phi * \text{calc\xi o}[P1, T1] + \text{calcD\xi oDP}[P1, T1])$

Out[660]= -0.253645

Term 3 ( $\delta T$ )

In[661]:=  $O3 = -VRdt * \phi m * S o1 * \text{calcD\xi oDT}[P1, T1]$

Out[661]= 6.16012

Term 4 ( $\delta S_o$ )

In[662]:=  $O4 = -VRdt * \phi m * \text{calc\xi o}[P1, T1]$

Out[662]= -15852.8

Term 5 ( $\ell$ )

In[663]:=  $O5 = VRdt * (\phi m * S o1 * \text{calc\xi o}[P1, T1])$

Out[663]= 12682.2

Term 6 (n)

In[664]:=  $O6 = -VRdt * (\phi m * S o1 * \text{calc\xi o}[P1, T1])$

Out[664]= -12682.2

Term 8 : 0 since  $\Delta D = 0$

In[665]:= O8 = 0

Out[665]= 0

Term 9, cell N production

In[666]:= O9c = - (-flowsource \* (calcffo @@ a1) \* (calcξo @@ a1))

Out[666]= 513.748

### ■ Energy Equation, LHS

Term 1 ( $\delta P$ )

In[668]:= E1 = (calcTw @@ a1) \* (calcξw @@ a1) \* (calcHwless @@ a1)

Out[668]= 0

**E19 = -E1**

**E23 = E1**

Term 2 ( $\delta P$ )

In[669]:= E2 = (calcTg @@ a1) \* (calcξg @@ a1) \* (calcHgmore @@ a1)

Out[669]= 0

**E20 = -E2**

**E24 = -E2**

Term 3 ( $\delta P$ )

In[670]:= E3 = (calcTo @@ a1) \* (calcξo @@ a1) \* (calcHo @@ a1)

Out[670]= 263.318

**E21 = -E3**

Term 4 ( $\delta T$ )

In[671]:= E4 = TE

Out[671]= 768.

**E22 = -E4**

Term 5 ( $\delta P$ )

In[672]:= E5 = -VRdt \* φm \* Sg1 \* (cφ \* calcξg[P1, T1] \* (calcUgmore @@ a1) +  
calcDξgDP[P1, T1] \* (calcUgmore @@ a1) + calcξg[P1, T1] \* (calcDUgmoreDP @@ a1))

Out[672]= 0

Term 6 ( $\delta P$ )

In[673]:= E6 = -VRdt \* φm \* Sw1 \* (cφ \* calcξw[P1, T1] \* (calcUwless @@ a1) +  
calcDξwDP[P1, T1] \* (calcUwless @@ a1) + calcξw[P1, T1] \* (calcDUwlessDP @@ a1))

Out[673]= -601.12

Term 7 ( $\delta P$ )

$$\text{In[674]:= } \mathbf{E7} = -\text{VRdt} * \phi_m * \text{Sol} * (\text{c}\phi * \text{calc}\xi_o[\text{P1}, \text{T1}] * (\text{calcUo} @@ \text{a11}) + \text{calcD}\xi_o\text{DP}[\text{P1}, \text{T1}] * (\text{calcUo} @@ \text{a11}) + \text{calc}\xi_o[\text{P1}, \text{T1}] * (\text{calcDUoDP} @@ \text{a11}))$$

Out[674]= -1509.32

Term 8 ( $\delta P$ )

$$\text{In[675]:= } \mathbf{E8} = \text{VRdt} * \phi_m * \text{c}\phi * \rho_R * \text{CR} * \text{T1}$$

Out[675]= 2101.2

Term 9 ( $\delta T$ )

$$\text{In[676]:= } \mathbf{E9} = -\text{VRdt} * \phi_m * \text{Sg1} * (\text{calcD}\xi_g\text{DT}[\text{P1}, \text{T1}] * (\text{calcUgmore} @@ \text{a11}) + \text{calc}\xi_g[\text{P1}, \text{T1}] * (\text{calcDUgmoreDT} @@ \text{a11}))$$

Out[676]= 0

Term 10 ( $\delta T$ )

$$\text{In[677]:= } \mathbf{E10} = -\text{VRdt} * \phi_m * \text{Sw1} * (\text{calcD}\xi_w\text{DT}[\text{P1}, \text{T1}] * (\text{calcUwless} @@ \text{a11}) + \text{calc}\xi_w[\text{P1}, \text{T1}] * (\text{calcDUwlessDT} @@ \text{a11}))$$

Out[677]=  $-3.84566 \times 10^6$

Term 11 ( $\delta T$ )

$$\text{In[678]:= } \mathbf{E11} = -\text{VRdt} * \phi_m * \text{Sol} * (\text{calcD}\xi_o\text{DT}[\text{P1}, \text{T1}] * (\text{calcUo} @@ \text{a11}) + \text{calc}\xi_o[\text{P1}, \text{T1}] * (\text{calcDUoDT} @@ \text{a11}))$$

Out[678]=  $-1.12453 \times 10^6$

Term 12 ( $\delta T$ )

$$\text{In[679]:= } \mathbf{E12} = -\text{VRdt} * (1 - \phi_m) * \rho_R * \text{CR}$$

Out[679]=  $-4.9028 \times 10^6$

Term 13 ( $\delta S_g$ )

$$\text{In[680]:= } \mathbf{E13} = \text{VRdt} * \phi_m * (\text{calc}\xi_w[\text{P1}, \text{T1}] \text{calcUwless}[\text{P1}, \text{T1}] - \text{calc}\xi_g[\text{P1}, \text{T1}] \text{calcUgmore}[\text{P1}, \text{T1}])$$

Out[680]=  $2.25015 \times 10^8$

Term 14 ( $\delta S_o$ )

$$\mathbf{E14} = \text{VRdt} * \phi_m * (\text{calc}\xi_w[\text{P1}, \text{T1}] \text{calcUwless}[\text{P1}, \text{T1}] - \text{calc}\xi_o[\text{P1}, \text{T1}] \text{calcUo}[\text{P1}, \text{T1}])$$

Out[681]=  $1.6211 \times 10^8$

### ■ Energy Equation, RHS

Term 15 ( $\ell$ )

$$\text{In[682]:= } \mathbf{E15} = \text{VRdt} * \phi_m * (\text{Sw1} * \text{calc}\xi_w[\text{P1}, \text{T1}] * \text{calcUwless}[\text{P1}, \text{T1}] + \text{Sol} * \text{calc}\xi_o[\text{P1}, \text{T1}] * \text{calcUo}[\text{P1}, \text{T1}] + \text{Sg1} * \text{calc}\xi_g[\text{P1}, \text{T1}] * \text{calcUgmore}[\text{P1}, \text{T1}])$$

Out[682]=  $1.28964 \times 10^8$

Term 16 (n)

$$\text{In}[683]:= \mathbf{E16} = -\mathbf{E15}$$

$$\text{Out}[683]= -1.28964 \times 10^8$$

Term 17 ( $\ell$ )

$$\text{In}[684]:= \mathbf{E17} = \mathbf{VRdt} * (1 - \phi_m) * \rho_R * \mathbf{CR} * \mathbf{T1}$$

$$\text{Out}[684]= 4.9028 \times 10^8$$

Term 18 (n)

$$\text{In}[685]:= \mathbf{E18} = -\mathbf{E17}$$

$$\text{Out}[685]= -4.9028 \times 10^8$$

Term 25,26,27 =0 since  $\Delta D=0$

$$\text{In}[686]:= \mathbf{E25} = \mathbf{E26} = \mathbf{E27} = 0$$

$$\text{Out}[686]= 0$$

Term 28-29, cell 1 injection

$$\text{In}[691]:= \mathbf{E28a} = -\mathbf{heatsource}$$

$$\text{Out}[691]= -1.94444 \times 10^6$$

Term 28-29, cell N production

$$\text{In}[693]:= \mathbf{E28c} = -(\mathbf{heatsource}) * ((\mathbf{calcffw} @@ \mathbf{a1}) * \mathbf{calc}\xi\mathbf{w}[\mathbf{P1}, \mathbf{T1}] * \mathbf{calcHwless}[\mathbf{P1}, \mathbf{T1}] +$$

$$(\mathbf{calcffo} @@ \mathbf{a1}) * \mathbf{calc}\xi\mathbf{o}[\mathbf{P1}, \mathbf{T1}] * \mathbf{calcHo}[\mathbf{P1}, \mathbf{T1}] +$$

$$(\mathbf{calcffg} @@ \mathbf{a1}) * \mathbf{calc}\xi\mathbf{g}[\mathbf{P1}, \mathbf{T1}] * \mathbf{calcHgmore}[\mathbf{P1}, \mathbf{T1}])$$

$$\text{Out}[693]= 3.12939 \times 10^9$$

Term 30, to boundaries

$$\text{In}[697]:= \mathbf{E30} = -(\mathbf{calcqb}[\mathbf{T1}] + \mathbf{calcqb}[\mathbf{T1}])$$

$$\text{Out}[697]= 0$$

## ■ Thermodynamic Constraints

Term 1;  $\delta P$

$$\text{In}[736]:= \mathbf{G1} = -1;$$

Term 2;  $\delta S_o$

$$\text{In}[737]:= \mathbf{G2} = \mathbf{calcDGDSO}[\mathbf{P1}, \mathbf{Ts1}, \mathbf{So1}, \mathbf{Sg1}, \mathbf{Sw1}]$$

$$\text{Out}[737]= -113.334$$

Term 3;  $\delta T_s$

$$\text{In}[738]:= \mathbf{G3} = \mathbf{calcDGDT}[\mathbf{P1}, \mathbf{Ts1}, \mathbf{So1}, \mathbf{Sg1}, \mathbf{Sw1}]$$

$$\text{Out}[738]= 4.55308$$

Term 4; ( $\ell$ )

```
In[740]:= G4 = - (calcG[P1, Ts1, Sol, Sg1, Sw1] + computePcown[Sw1])
```

```
Out[740]= 18.9989
```

■ **At T=500F, P=500**

---