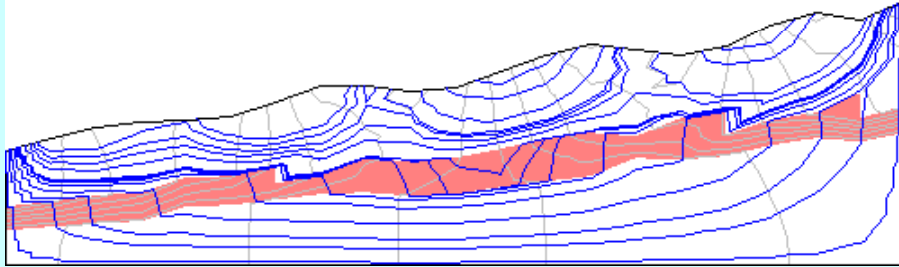
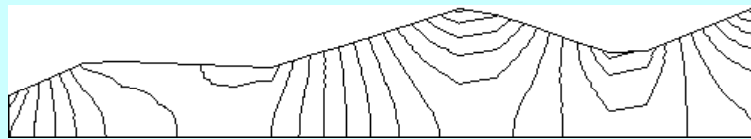


UPPER BOUNDARY IS
CONSTANT HEAD
EQUAL TO WATER TABLE ELEVATION
LIKE MANY RESERVOIRS PROVIDING AND RECEIVING WATER
no exaggeration -- head distribution
with aquitard

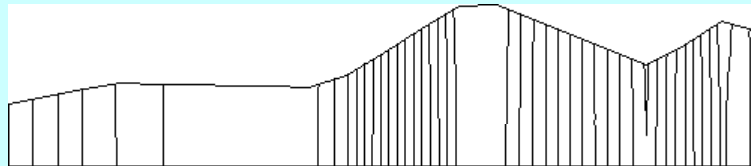


NOTE THAT
POROSITY DOES NOT EFFECT FLOW FIELD
IT ONLY CHANGES TRAVEL TIME

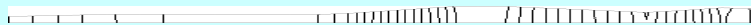
no exaggeration -- head distribution

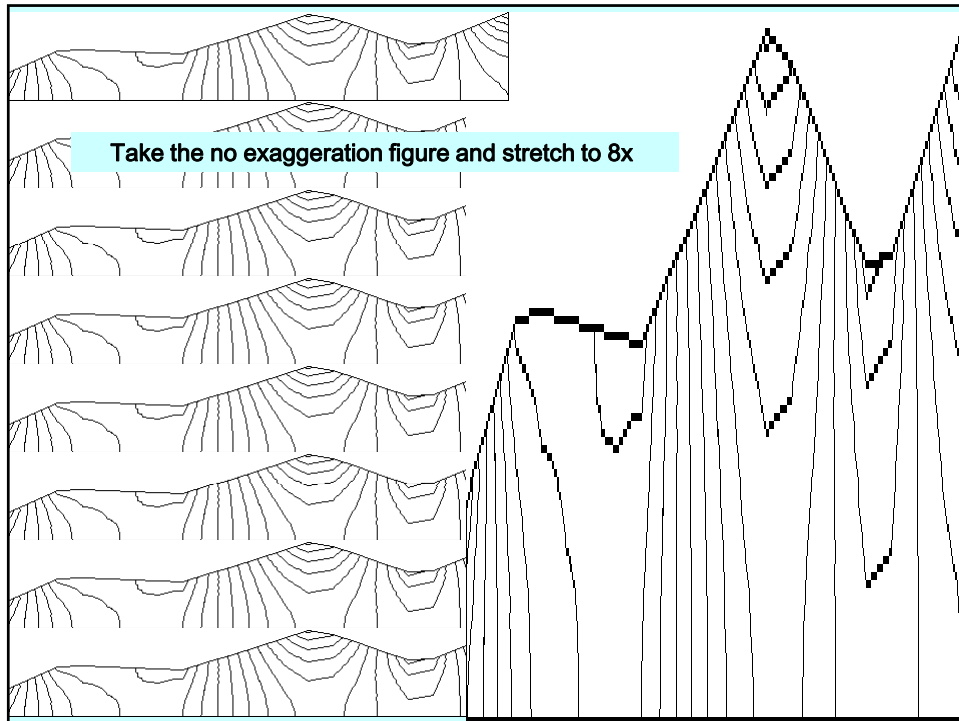


draw similar shape but under 10x exaggeration -- head distribution



Take the 10x exaggeration figure and shrink to 0.1x





try it for $K_x = 16 \text{ ft/day}$ and $K_z = 4 \text{ ft/day}$

- 1 - Draw an INVERSE K ellipse for semi-axes $\frac{1}{\sqrt{K_x}}$ and $\frac{1}{\sqrt{K_z}}$
- 2 - Draw the direction of the hydraulic gradient through the ellipse and note where it intercepts the ellipse
- 3 - Draw the tangent to the ellipse at this point
- 4 - Flow direction is perpendicular to this line

http://inside.mines.edu/~epoeter/_GW/09FlowNets/Exercises_9ckey.html

http://inside.mines.edu/~epoeter/_GW/09FlowNets/Exercises_9dkey.html

A PLAN VIEW FLOW NET BY CONTOURING USING FIELD HEADS AND DRAWING FLOW LINES PERPENDICULAR: can't assume constant K or b assuming no inflow from above or below, we can evaluate relative T:

$$Q = A_A V_1 = A_B V_2$$

$$A_A K_A \frac{\Delta h}{l_A} = A_B K_B \frac{\Delta h}{l_B}$$

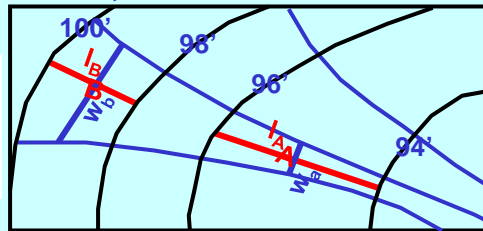
$$\frac{A_A K_A}{l_A} = \frac{A_B K_B}{l_B} \quad \frac{K_A}{K_B} = \frac{A_B l_A}{A_A l_B}$$

$A = wb$ (b = aquifer thickness)

$$\frac{K_A}{K_B} = \frac{w_B b_B l_A}{w_A b_A l_B}$$

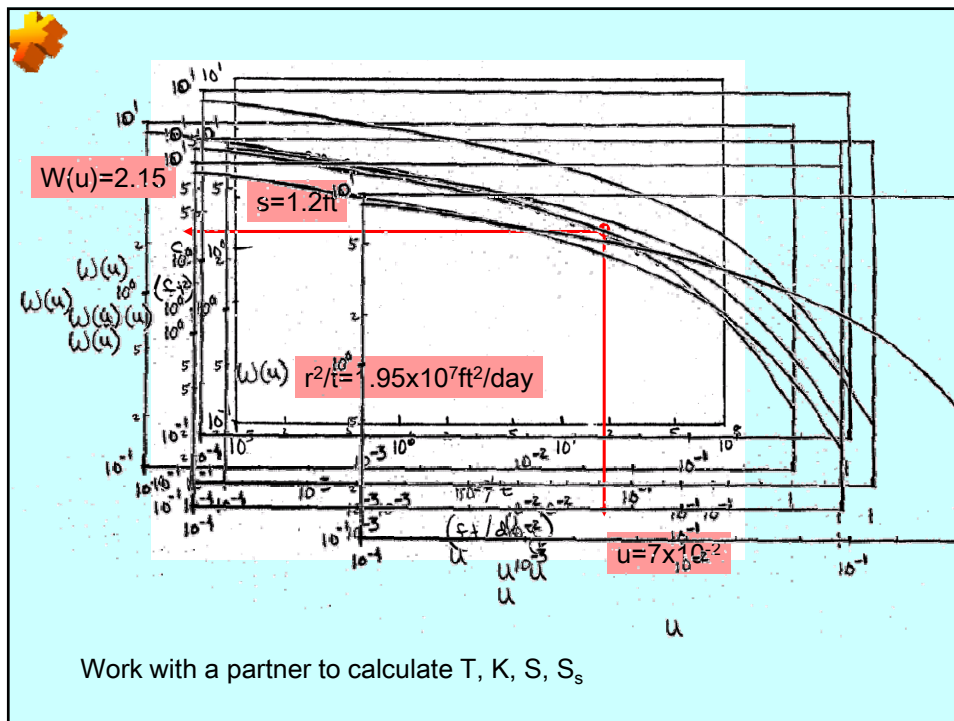
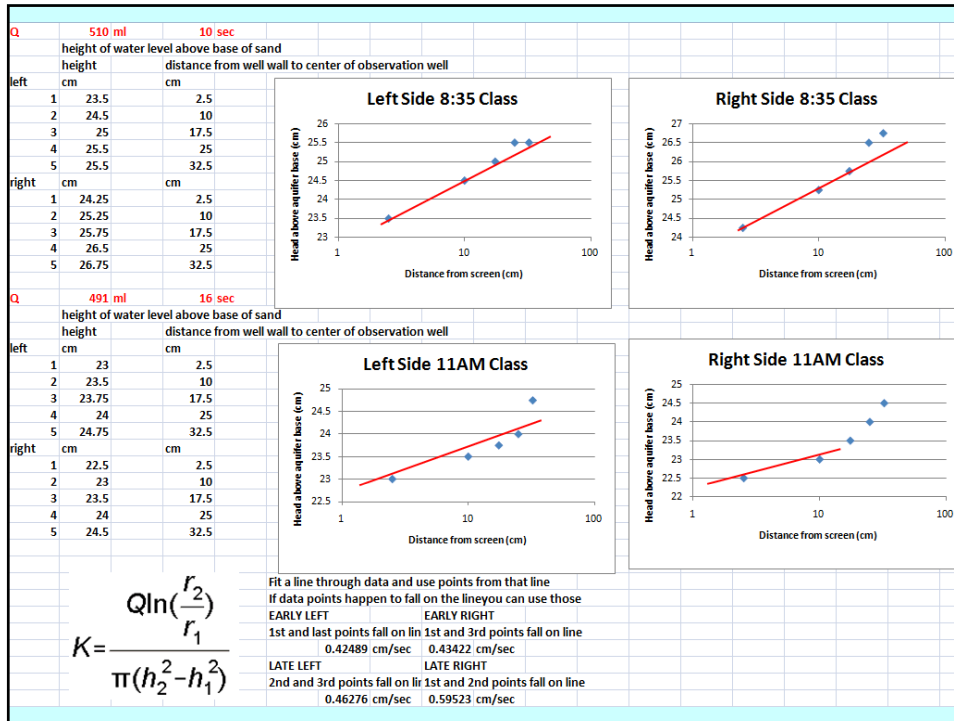
$$\frac{K_A b_A}{K_B b_B} = \frac{w_B l_A}{w_A l_B} = \frac{T_A}{T_B}$$

$$\frac{K_A b_A}{K_B b_B} = \frac{w_B l_A}{w_A l_B} = \frac{T_A}{T_B}$$



"Irregularities" in "Natural" flow nets

varying K
 varying flow thickness
 recharge/discharge
 vertical components of flow
 Nature's flow nets provide
 clues to
 geohydrologic conditions



$T = \frac{Q}{4\pi s} W(u) = \frac{500 \frac{\text{gal}}{\text{min}} \frac{1 \text{ft}^3}{7.48 \text{gal}} \frac{60(24) \text{min}}{\text{day}} \cdot 2.15}{4\pi \cdot 1.2 \text{ft}} = 13724 \text{ft}^2/\text{day} \approx 1.4 \times 10^4 \frac{\text{ft}^2}{\text{day}}$

$K = T/b = 140 \text{ft/day}$

$S = \frac{4Tu}{(r^2/t)} = \frac{4(13724 \text{ft}^2/\text{day})(7 \times 10^{-2})}{1.95 \times 10^7 \text{ft}^2/\text{day}} = 2 \times 10^{-4}$

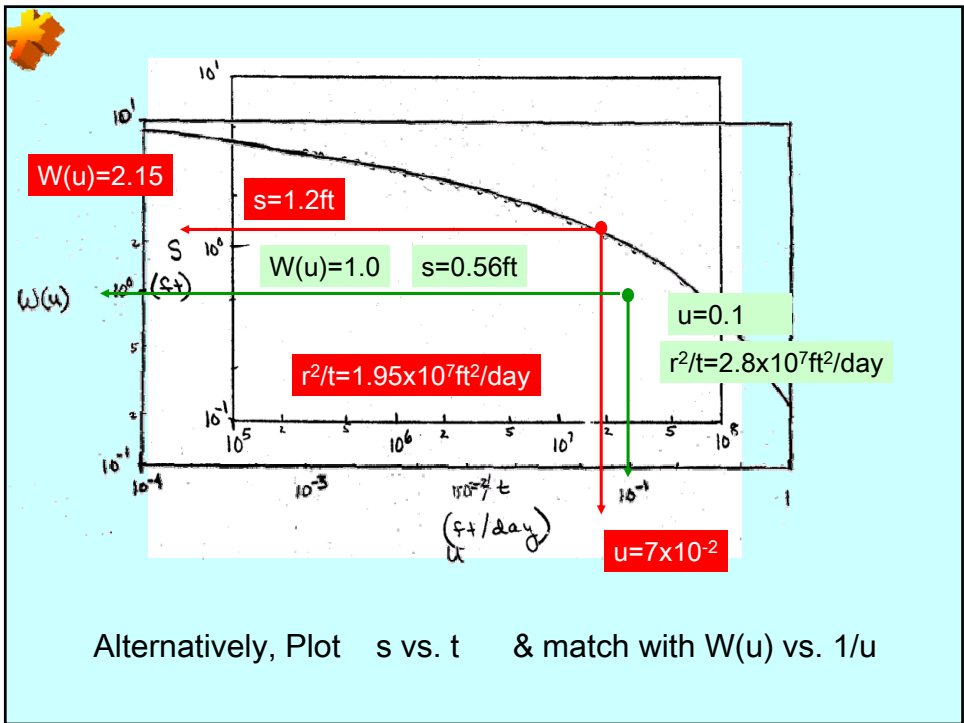
specific storage = $\frac{S}{b} = 2 \times 10^{-6} \text{ft}^{-1}$

Any point can be used. It need not be on the curve. Why?
 (see next slide)

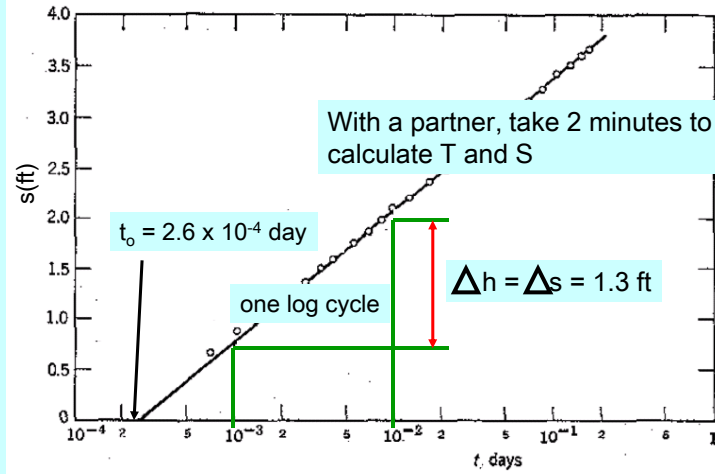
$W(u) = 1$ $s = 0.56$
 $u = 0.1$ $r^2/t = 2.8 \times 10^7$

$T = 13678 \text{ft}^2/\text{day}$ approx. $1.4 \times 10^4 \text{ft}^2/\text{day}$
 $S = 1.95 \times 10^{-4}$ approx. 2×10^{-4}

The curve match identifies the appropriate relative values.



For the Ohio example $Q=500\text{GPM}$, $b=100\text{ft}$, $r=200\text{ft}$
 Plot s vs t



$$T = \frac{2.3Q}{4\pi\Delta h} \quad S = \frac{2.25Tt_0}{r^2}$$



$$T = \frac{2.3Q}{4\pi\Delta h}$$

Δh = drawdown over 1 log cycle of time

$$= \frac{(2.3) 500 \frac{\text{gal}}{\text{min}} \frac{1\text{ft}^3}{7.48\text{gal}} \frac{60(24)\text{min}}{\text{day}}}{4\pi 1.3\text{ft}}$$

$$= 13,552 \text{ ft}^2/\text{day} \sim 1.4 \times 10^4 \text{ ft}^2/\text{day}$$

$$S = \frac{2.25Tt_0}{r^2}$$

t_0 = time intercept for zero drawdown

$$= \frac{2.25 * 13,552 \text{ ft}^2/\text{day} * 2.6 \times 10^{-4} \text{ day}}{(200\text{ft})^2}$$

$$= \sim 1.98 \times 10^{-4} \sim 2 \times 10^{-4}$$