

After 10 days

$$u_{10\text{days}} = (r^2 S) / (4T t) = ((100\text{ft})^2 1 \times 10^{-5}) / (4 \cdot 1 \text{ ft}^2 / \text{day} \cdot 10\text{day})$$

$$= 2.5 \times 10^{-3}$$

$$W(u)_{10\text{days}} \sim 5.44$$

$$S_{40\text{cfd}10\text{days}} = (Q W(u)) / (4\pi T) = (40 \text{ ft}^3 / \text{day} \cdot 5.44) / (4 \pi \cdot 1 \text{ ft}^2 / \text{day})$$

$$S_{40\text{cfd}10\text{days}} = 17.3 \text{ ft}$$

After 5 days

$$u_{5\text{days}} = (r^2 S) / (4T t) = ((100\text{ft})^2 1 \times 10^{-5}) / (4 \cdot 1 \text{ ft}^2 / \text{day} \cdot 5\text{day})$$

$$= ((100)^2 \cdot 5 \times 10^{-7})$$

$$= 5 \times 10^{-3}$$

$$W(u)_{5\text{days}} \sim 4.73$$

$$S_{30\text{cfd}5\text{days}} = (Q W(u)) / (4\pi T) = (30 \text{ ft}^3 / \text{day} \cdot 4.73) / (4 \pi \cdot 1 \text{ ft}^2 / \text{day})$$

$$S_{30\text{cfd}5\text{days}} = -11.3 \text{ ft}$$

$S_{40\text{cfd}5\text{days} \& 10\text{cfd}5\text{days}} = 6 \text{ ft}$

location of interest

r = 100ft

pumping well

Plan View

$T = 1 \times 10^0 \text{ ft}^2 / \text{day}$ $S = 1 \times 10^{-5}$

$Q = 40 \text{ ft}^3 / \text{day}$ for 5 day

$Q = 10 \text{ ft}^3 / \text{day}$ for the next 5 days

Pumping continues for 10 days

What is specific capacity?

Specific capacity is short term sustainable discharge divided by the drawdown yielding the discharge (typically in GPM/ft)

Where do we get specific capacity?

Drillers measure specific capacity and report it on well logs that we obtain from the State Engineer. They typically blow air in the borehole to obtain the discharge for about 4 hours. They often use total depth for the maximum water depth. It is not unusual for them to “cheat” on the duration of the test.

Why do we want to calculate Transmissivity from specific capacity?

Specific capacity data are readily available at many locations in a basin. For little effort (compared to conducting an aquifer test) we can obtain an approximation of transmissivity and its distribution.

If $K_H = 4$ $K_V = 1$ $b = 200$ ft
 How far must I be from the well to avoid affects of partial penetration?
 If $K_H = 4$ $K_V = 1$ $b = 200$ ft
 $r = 1.5 * (200\text{ft}) * 2 = 600$ ft

Assuming this diagram is drawn to scale, what is the ratio of K_H/K_V ?
 The ratio of K_H/K_V is approximately 1 because the lines of equal head are vertical starting about 1.5 aquifer thicknesses from the well bore.
 At which location will the error be greatest if you do not account for partial penetration? 1, 2, 3, or 4? How do you know?
 Discuss with your neighbors.
 furthest vertically from the well thus causing the greatest deviation from a fully penetrating situation.

Using data from the sand tank on the next sheet
 Estimate K via Hvorslev AND Bouwer and Rice Methods
 How do the K values compare? And for the pump test we did earlier in the semester?
 How does the tank fit the assumptions of the methods?

$$K = \frac{r^2 \ln\left(\frac{L_e}{R}\right)}{2 L_e T_0}$$

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{R}\right)}{2 L_e} \frac{1}{t} \ln\left(\frac{H_o}{H_t}\right)$$

$$\text{for } L_w < h \ln\left(\frac{R_e}{R}\right) = \left[\frac{11}{\ln\left(\frac{L_w}{R}\right)} + \frac{A+B \ln\left(\frac{h-L_w}{R}\right)}{\frac{L_w}{R}} \right]^{-1}$$

$$\text{for } L_w = h \ln\left(\frac{R_e}{R}\right) = \left[\frac{11}{\ln\left(\frac{L_w}{R}\right)} + \frac{C}{\frac{L_w}{R}} \right]^{-1}$$

| | Time since slug sec | h above initial water level cm |
|---|------------------------|-----------------------------------|
|  <p> Bore radius = 4.9cm Screen Length = 6cm Saturated thickness = 30cm </p> | | 6.6 |
| | 2 | 6 |
| | 4 | 4.6 |
| | 6 | 3.6 |
| | 8 | 3 |
| | 10 | 2.6 |
| | 12 | 2.2 |
| | 14 | 1.9 |
| | 16 | 1.65 |
| | 18 | 1.5 |