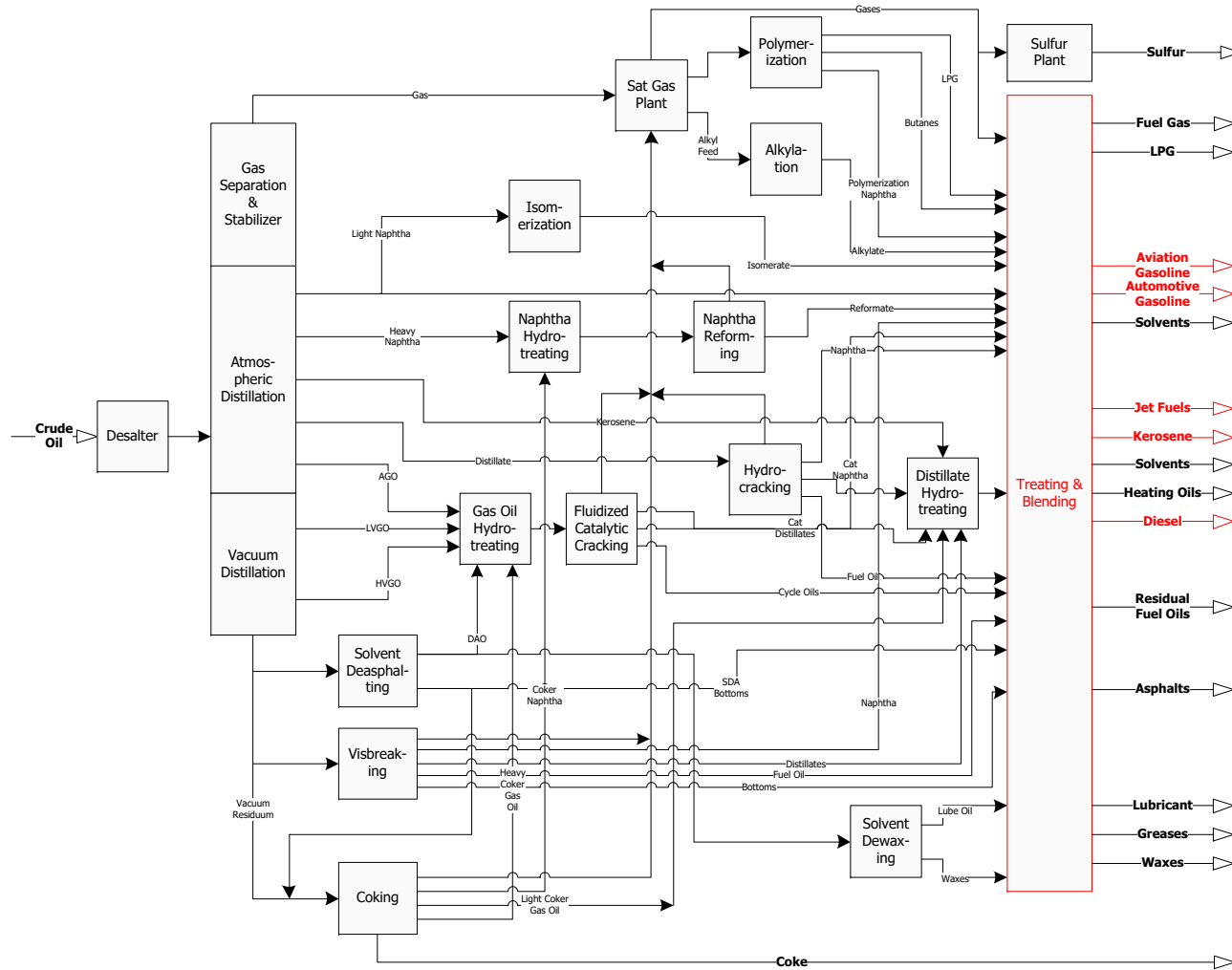


# Product Blending & Optimization Considerations

Chapters 12 & 14





# Topics

## Blending

- Blending equations
- Specifications / targets
- Typical blend stock properties

## Optimization

- Economics & planning applications
- Optimization tools
  - Linear programming
  - Non-linear (geometric) programming

Adjusting upstream operations to meet downstream targets

# Blending

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# Blending Equations

## Volume blending equations

- Specific gravity
- Aromatics & olefins content (vol%)

$$X_{mix} = \sum v_i X_i = \frac{\sum v_i X_i}{\sum v_i}$$

## Mass blending equations

- Sulfur & nitrogen content (wt% or ppm)
- Nickel & vanadium (ppm)
- Carbon residue (CCR, MCRT, ...)

$$X_{mix} = \sum w_i X_i = \frac{\sum v_i \gamma_{oi} X_i}{\sum v_i \gamma_{oi}}$$

## Reid Vapor Pressure (RVP)

$$(RVP)_{mix}^{1.25} = \frac{\sum V_i (RVP)_i^{1.25}}{\sum V_i}$$

## Octane numbers – Simple, by volume

$$(RON)_{mix} = \frac{\sum V_i (RON)_i}{\sum V_i}$$

$$(MON)_{mix} = \frac{\sum V_i (MON)_i}{\sum V_i}$$

## Viscosity

$$\log(\log(v_{mix} + 0.7)) = \frac{\sum V_i \log(\log(v_i + 0.7))}{\sum V_i}$$

# Non-Linear Octane Blending Formula

Developed by Ethyl Corporation using a set of 75 & 135 blends

$$R = \bar{R} + a_1 [\overline{RJ} - \bar{R} \times \bar{J}] + a_2 \left[ \overline{(O^2)} - \bar{O}^2 \right] + a_3 \left[ \overline{(A^2)} - \bar{A}^2 \right]$$

$$M = \bar{M} + b_1 [\overline{MJ} - \bar{M} \times \bar{J}] + b_2 \left[ \overline{(O^2)} - \bar{O}^2 \right] + b_3 \left[ \frac{\overline{(A^2)} - \bar{A}^2}{100} \right]^2$$

$$\text{"Road" Octane} = \frac{R + M}{2}$$

$$\text{Sensitivity} = J \equiv R - M$$

$$\text{Volume Average} = \bar{X} \equiv \frac{\sum V_i \times X_i}{\sum V_i}$$

	75 blends	135 blends
$a_1$	0.03224	0.03324
$a_2$	0.00101	0.00085
$a_3$	0	0
$b_1$	0.04450	0.04285
$b_2$	0.00081	0.00066
$b_3$	-0.00645	-0.00632

*Petroleum Refinery Process Economics*, 2<sup>nd</sup> ed. ,  
by Robert E. Maples, PennWell Corp., 2000

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# Typical Gasoline Blend Stock Properties

No.	Component	RVP, psi	(R+M)/2	MON	RON	°API
1	iC4	71.0	92.5	92.0	93.0	
2	nC4	52.0	92.5	92.0	93.0	
3	iC5	19.4	92.0	90.8	93.2	
4	nC5	14.7	72.0	72.4	71.5	
5	iC6	6.4	78.8	78.4	79.2	
6	LSR gasoline (C5-180°F)	11.1	64.0	61.6	66.4	78.6
7	LSR gasoline isomerized once-through	13.5	82.1	81.1	83.0	80.4
8	HSR gasoline	1.0	60.5	58.7	62.3	48.2
9	Light hydrocrackate	12.9	82.6	82.4	82.8	79.0
10	Hydrocrackate, C5-C6	15.5	87.4	85.5	89.2	86.4
11	Hydrocrackate, C6-190°F	3.9	74.6	73.7	75.5	85.0
12	Hydrocrackate, 190-250°F	1.7	77.3	75.6	79.0	55.5
13	Heavy hydrocrackate	1.1	67.5	67.3	67.6	49.0
14	Coker gasoline	3.6	63.7	60.2	67.2	57.2
15	Light thermal gasoline	9.9	76.8	73.2	80.3	74.0
16	C6+ light thermal gasoline	1.1	72.5	68.1	76.8	55.1
17	FCC gasoline, 200-300°F	1.4	84.6	77.1	92.1	49.5
18	Hydrog. light FCC gasoline, C5+	13.9	82.1	80.9	83.2	51.5
19	Hydrog. C5-200°F FCC gasoline	14.1	86.5	81.7	91.2	58.1
20	Hydrog. light FCC gasoline, C6+	5.0	80.2	74.0	86.3	49.3
21	Hydrog. C5+ FCC gasoline	13.1	85.9	80.7	91.0	54.8
22	Hydrog. 300-400°F FCC gasoline	0.5	85.8	81.3	90.2	48.5
23	Reformate, 94 RON	2.8	89.2	84.4	94.0	45.8
24	Reformate, 98 RON	2.2	92.3	86.5	98.0	43.1
25	Reformate, 100 RON	3.2	94.1	88.2	100.0	41.2
26	Aromatic concentrate	1.1	100.5	94.0	107.0	
27	Alkylate, C3=	5.7	89.1	87.3	90.8	
28	Alkylate, C4=	4.6	96.6	95.9	97.3	70.3
29	Alkylate, C3=, C4=	5.0	93.8	93.0	94.5	
30	Alkylate, C5=	1.0	89.3	88.8	89.7	
31	Polymer	8.7	90.5	84.0	96.9	59.5

**Table 12.1 Blending Component Values for Gasoline Blending Streams**

*Petroleum Refining Technology & Economics – 5<sup>th</sup> Ed.*

by James Gary, Glenn Handwerk, & Mark Kaiser, CRC Press, 2007

Updated: July 12, 2018

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# Gasoline Blending Considerations

## What is available?

- Amounts
- Properties
  - Appropriate to determine product properties
- Associated costs / values

## What are you trying to make?

- Amount(s)
- Properties
  - Volatility / RVP (maximum)
  - Octane number (minimum)
  - Drivability Index
  - Distillation
    - T10 (minimum)
    - T50 (range)
    - T90 (maximum)
  - Composition
    - Sulfur (maximum)
    - Benzene & total aromatics (maximums)
    - Olefins (maximum)
- Value

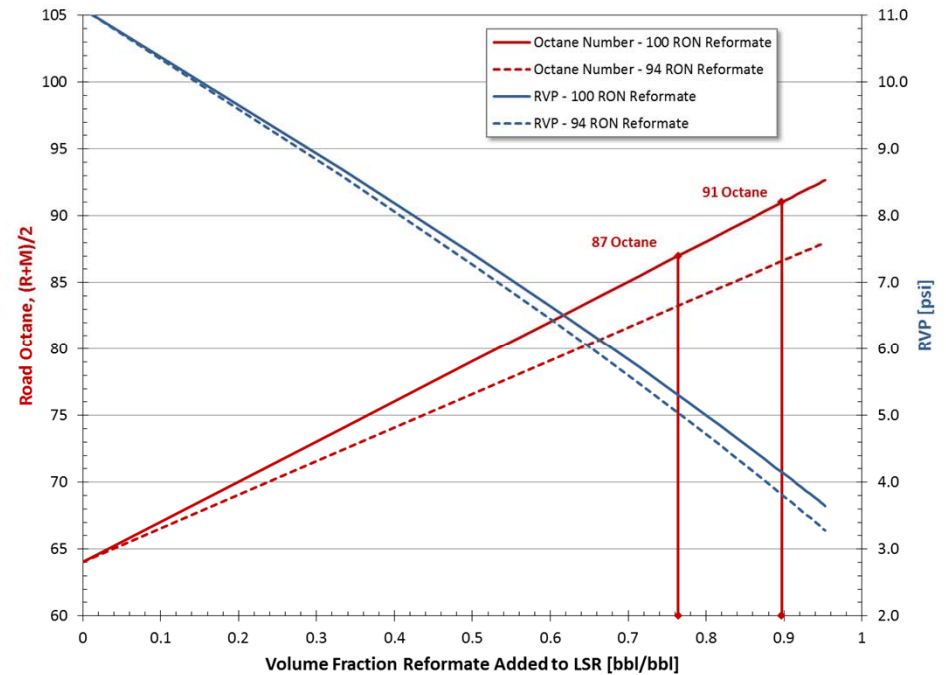
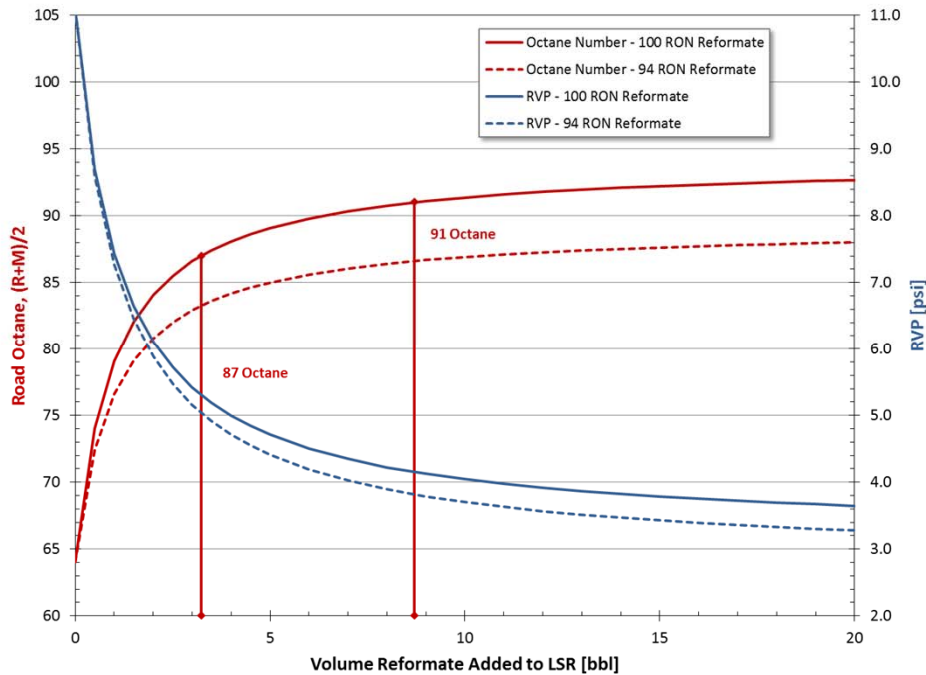


# Gasoline Blend Example – 2 Blend Stocks, 1 Spec

Example, blending LSR only with Reformate – one case 100 RON, other 94 RON

To make Regular or Premium spec, essentially diluting the Reformate

- 94 RON Reformate alone cannot bring LSR up to final spec



# Gasoline Blend Example – 3 Blend Stocks, 2 Specs

Use 3 blend stocks to make regular gasoline (87 road octane) for both summer (9 psi RVP) & winter (15 psi RVP)

$$\left(\frac{R+M}{2}\right) = (92.5)v_{nC4} + (64.0)v_{LSR} + (94.1)v_{Ref}$$

$$(RVP)^{1.25} = (71.0)^{1.25} v_{nC4} + (11.1)^{1.25} v_{LSR} + (3.2)^{1.25} v_{Ref}$$

$$1 = v_{nC4} + v_{LSR} + v_{Ref}$$

	Blend Stocks			Regular, no nC4	Regular Summer	Regular Winter
Volume Fractions:						
n-Butane	1				0.038	0.107
LSR (C5 - 180°F)		1		0.236	0.234	0.230
Reformat, 100 RON			1	0.764	0.729	0.663
RVP [psi]	71.0	11.1	3.2	5.3	9.0	15.0
RON	93.0	66.4	100.0	92.1	91.9	91.5
MON	92.0	61.6	88.2	81.9	82.1	82.5
(R+M)/2	92.5	64.0	94.1	87.0	87.0	87.0
Volume Ratios:						
Total:LSR				4.2	4.3	4.3
Reformat:LSR				3.2	3.1	2.9

# Diesel Blending Considerations

## Available blend stocks

- Amounts
- Properties
  - Appropriate to determine product properties
- Associated costs / values

## Specification of final product(s)

- Amount(s)
- Properties
  - Cetane index (minimum)
  - Flash Point (minimum)
  - Distillation
    - T90 (minimum & maximum)
  - Cold properties
    - Cloud point (minimum)
    - Pour point (minimum)
  - Composition
    - Sulfur (maximum)
    - Aromaticity (maximum)
    - Carbon residue (maximum)
  - Color
- Value

# Optimization

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# Optimization for Economics & Planning

What *should* be done rather than what *can* be done

## Optimization

- Combines models to...
  - Describe operations
  - Constraints to operations
- Economics added to define costs & benefits to all actions
- “Optimal” is best of the “feasible” possibilities

Optimization models tend to be data-driven rather than mathematical model driven.

# Economics & Planning Applications

## Crude oil evaluation

- Incremental value of an opportunity crude compared to base slate
- Take into account change in products produced

## Production planning

## Day-to-day operations optimization

## Product blending & pricing

- May have opportunity to separately purchase blend stocks

## Shutdown planning

- Multi time periods, must take into account changes in inventories

## Multirefining supply & distribution

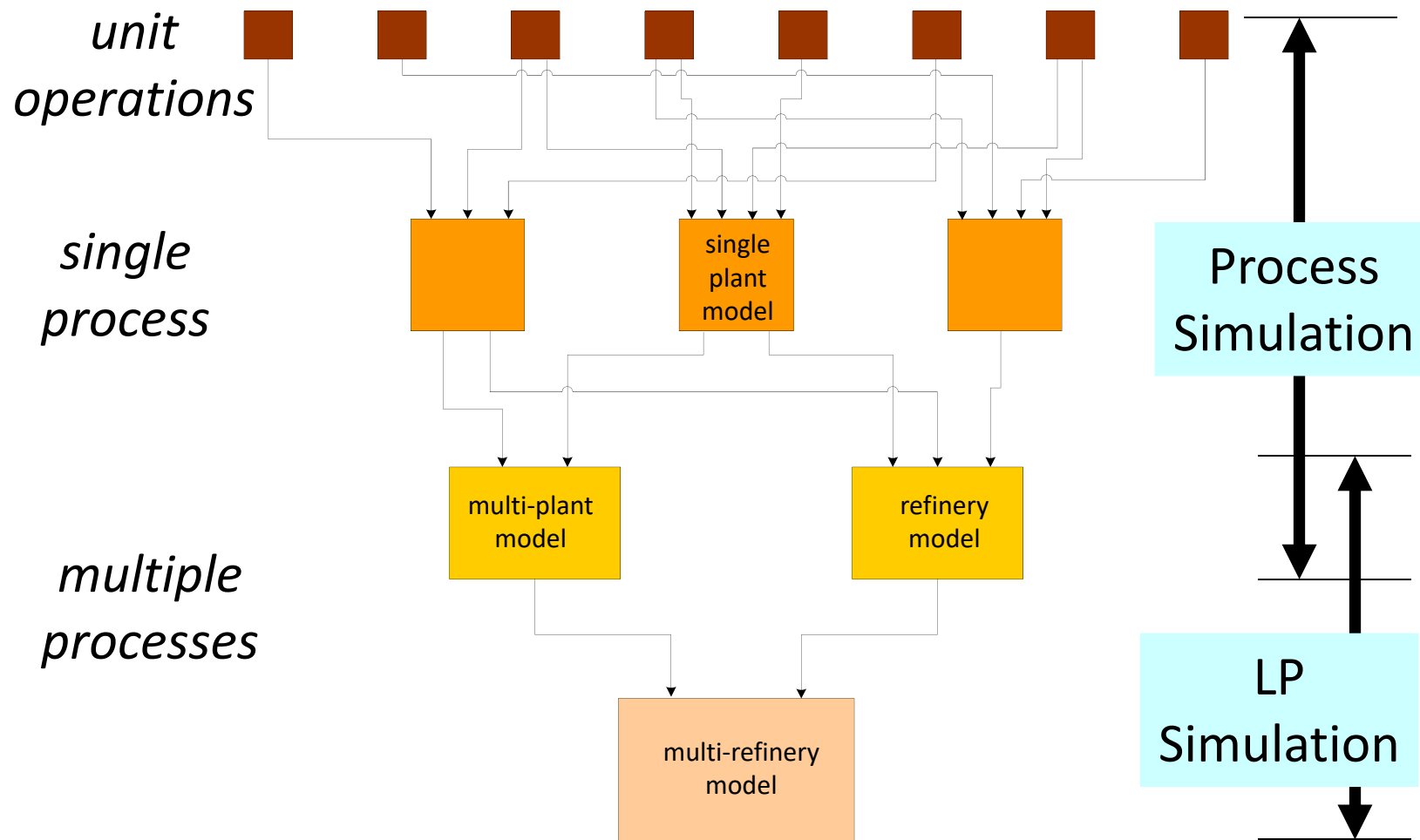
## Yearly budgeting

## Investment studies

## Environmental studies

## Technology evaluation

# Modeling Hierarchy



# Unit Representations

## Simple vector model

	Yield Vector
Feedstock	
Butylene	-1.0000
Isobutane	-1.2000
Product	
n-Butane	0.1271
Pentane	0.0680
Alkylate	1.5110
"Alky Bottoms	0.1190
Tar	0.0096
Utilities	
Steam, lb	7.28
Power, kWh	2.45
Cooling Water, M gal	2.48
Fuel, MMBtu	0.69

For every unit of Butylene consumed, must also consume the relative amount of isobutane, produce the shown amounts of products, & use the shown amounts of utilities

## Delta-Base model

	Feed	Base Yield	Delta Kw	Delta API
Feed	1.0	-1.0		
Hydrogen		-1500		
C5-180		8.1	1.0	3.6
180-400		28.0	-5.5	11.0
Kw	-12.1	10.9	1.2	
API	-22.0	20.0		4.0
Relative Activity	1	1	1	0.5

Relative activities calculated from actual properties – the Kw & API rows are zero

$$API = -\frac{1 \times (-22.0) + 1 \times 20.0}{4.0} = 0.5$$

Correct base yields to take into account actual properties & relative activities

$$C5-180 = \frac{1 \times 8.1 + 1 \times 1.0 + 0.5 \times 3.6}{1} = 10.9$$



# What is “Linear Programming”?

Word “programming” used here in the sense of “planning”

For N independent variables (that can be zero or positive) **maximize**

$$z = a_{01}x_1 + a_{02}x_2 + \cdots + a_{0N}x_N$$

subject to M additional constraints (all  $b_n$  positive)

$$a_{i1}x_1 + a_{i2}x_2 + \cdots + a_{iN}x_N \leq b_i$$

$$a_{j1}x_1 + a_{j2}x_2 + \cdots + a_{jN}x_N \geq b_j$$

$$a_{k1}x_1 + a_{k2}x_2 + \cdots + a_{kN}x_N = b_k$$

## Terminology

- Objective Function – function  $z$  to be maximized
- Feasible Vector – set of values  $x_1, x_2, \dots, x_N$  that satisfies all constraints
- Optimal Feasible Vector – feasible vector that maximizes the objective function

## Solutions

- Will tend to be in the “corners” of where the constraints meet
- May not have a solution because of incompatible constraints or area unbounded towards the optimum

# Change Blending Equations to Fit Linear Form

Sum of blending factors must be removed from the denominator

- Volume blending equations

$$X_{mix} = \frac{\sum v_i X_i}{\sum v_i} \Rightarrow 0 = \sum v_i (X_i - X_{mix})$$

- Mass blending equations

$$X_{mix} = \frac{\sum w_i X_i}{\sum w_i} = \frac{\sum v_i \gamma_{oi} X_i}{\sum v_i \gamma_{oi}} \Rightarrow 0 = \sum v_i [\gamma_{oi} (X_i - X_{mix})]$$

# Non-Linear Programming

Non-linear blending rules can more closely match the physics of the problem

- Example: octane blending models

$$R = \bar{R} + 0.03324 \left[ \overline{RJ} - \bar{R} \cdot \bar{J} \right] + 0.00085 \left[ \overline{(O^2)} - \bar{O}^2 \right]$$

$$M = \bar{M} + 0.04285 \left[ \overline{MJ} - \bar{M} \cdot \bar{J} \right] + 0.00066 \left[ \overline{(O^2)} - \bar{O}^2 \right] - 6.32 \times 10^{-7} \left[ \overline{(A^2)} - \bar{A}^2 \right]$$

Guarantees of solutions are more tenuous

- Not necessarily at constraints
- Discontinuous feasible regions possible

Types of optimization algorithms

- Local optimization
  - Based on following gradients
    - Excel's Solver based on GRG2
- Global optimization
  - Randomly search overall region before switching to local optimization technique
    - Simulated annealing

# Blending Example with Optimization

Brewery receives order for 100 gal of 4% beer. Only have in stock 4.5% & 3.7% beers (beers A & B). Will make order by mixing these two beers and water at minimum ingredient cost.

- Values:

Beer A	\$0.32 per gallon
Beer B	\$0.25 per gallon
Water	No cost

- Constraints:

At least 10 gal Beer A

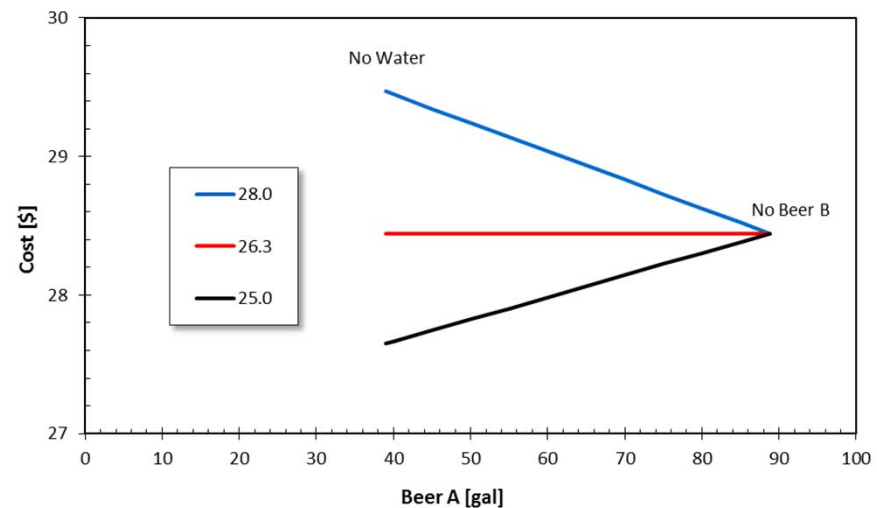
- Extreme solutions:

A	88.9	gallons
B	0	gallons
Water	11.1	gallons
A	37.5	gallons
B	62.5	gallons
Water	0	gallons

- Associated costs:

No Beer B	\$28.44
No Water	\$27.63

Beer A — 32 ¢/gal  
 Beer B/Water Mixed to Make 100 gal & 4% Sales Beer Specs  
 Legend — Beer B Cost (¢/gal)



# Gasoline Blending Considerations

## What is available?

- Amounts
- Properties
  - Appropriate to determine product properties
- Associated costs / values

## What are you trying to make?

- Amount(s)
- Properties
  - Volatility / RVP (maximum)
  - Octane number (minimum)
  - Drivability Index
  - Distillation
    - T10 (minimum)
    - T50 (range)
    - T90 (maximum)
  - Composition
    - Sulfur (maximum)
    - Benzene & total aromatics (maximums)
    - Olefins (maximum)
- Value

# Gasoline Blending Example – All Into Regular

<i>Raw Materials</i>	<i>Properties for Blending Calculations</i>							
	RON	MON	(R+M)/2	RVP	RVP <sup>1.25</sup>	Aromatics	Olefins	Benzene
Butane	93.0	92.0	92.5	54	146.4	0.0	0.0	0.00
Straight Run Naphtha	78.0	76.0	77	11.2	20.5	2.2	0.9	0.73
Isomerate	83.0	81.1	82.05	13.5	25.9	1.6	0.1	0.00
Reformate (High Octane)	100.0	88.2	94.1	3.2	4.3	94.2	0.6	1.85
Reformate (Low Benzene)	93.7	84.0	88.85	2.8	3.6	61.1	1.0	0.12
FCC Naphtha	92.1	77.1	84.6	1.4	1.5	35.2	32.6	1.06
Alkylate	97.3	95.9	96.6	4.6	6.7	0.5	0.2	0.00

	<i>Cost &amp; Availability</i>			<i>Usage</i>				
	Cost (\$/gal)	Minimum Required	Maximum Available	Regular	Premium	Total	Minimum Slack	Maximum Slack
Butane	<b>0.85</b>	<b>0</b>	<b>30,000</b>	<b>30,000</b>	<b>0</b>	30,000	<b>30,000</b>	<b>0</b>
Straight Run Naphtha	<b>2.05</b>	<b>0</b>	<b>35,000</b>	<b>35,000</b>	<b>0</b>	35,000	<b>35,000</b>	<b>0</b>
Isomerate	<b>2.20</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	0	<b>0</b>	<b>0</b>
Reformate (High Octane)	<b>2.80</b>	<b>0</b>	<b>60,000</b>	<b>60,000</b>	<b>0</b>	60,000	<b>60,000</b>	<b>0</b>
Reformate (Low Benzene)	<b>2.75</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	0	<b>0</b>	<b>0</b>
FCC Naphtha	<b>2.60</b>	<b>0</b>	<b>70,000</b>	<b>70,000</b>	<b>0</b>	70,000	<b>70,000</b>	<b>0</b>
Alkylate	<b>2.75</b>	<b>0</b>	<b>40,000</b>	<b>40,000</b>	<b>0</b>	40,000	<b>40,000</b>	<b>0</b>

<i>Products</i>		<i>Lower &amp; Upper Limits on Properties</i>	
		Lower	Upper
Regular	Octane	<b>87</b>	<b>110</b>
	RVP	<b>0.0</b>	<b>15.0</b>
	RVP <sup>1.25</sup>	0.0	29.5
Premium	Benzene	<b>0.0</b>	<b>1.1</b>
	Octane	<b>91</b>	<b>110</b>
	RVP	<b>0.0</b>	<b>15.0</b>
	RVP <sup>1.25</sup>	0.0	29.5
	Benzene	<b>0.0</b>	<b>1.1</b>

	<i>Price &amp; Production Requirements</i>		
	Price (\$/gal)	Minimum Required	Maximum Allowed
Regular	<b>2.75</b>	<b>1</b>	<b>1,000,000</b>
Premium	<b>2.85</b>	<b>1</b>	<b>1</b>

<i>Cost &amp; Revenue</i>			
Revenue (\$)	\$646,250	\$1	\$646,251
Cost(\$)	\$557,250	\$1	\$557,251
Profit (\$)	\$89,000	\$0	<b>\$89,000</b>

<i>Product Calculations</i>	<i>Volumes &amp; Properties</i>		
	Regular	Premium	Total
Produced	<b>235,000</b>	<b>0</b>	235,000
RON	93.02	83.24	
MON	84.87	81.59	
(R+M)/2	<b>88.9</b>	<b>82.4</b>	
RVP	<b>12.9</b>	<b>28.0</b>	
RVP <sup>1.25</sup>	24.43	64.46	
Benzene	<b>0.90</b>	<b>0.48</b>	

		<i>Linear-Form Product Constraints</i>	
		Lower Slack	Upper Slack
Regular	Volume	<b>234,999</b>	<b>765,000</b>
	Vol*Octane	<b>457,000</b>	<b>4,948,000</b>
	Vol*RVP <sup>1.25</sup>	<b>5,741,488</b>	<b>1,195,675</b>
	Vol*Benzene	<b>210,750</b>	<b>47,750</b>
Premium	Volume	<b>-1</b>	<b>1</b>
	Vol*Octane	<b>-3</b>	<b>11</b>
	Vol*RVP <sup>1.25</sup>	<b>25</b>	<b>-14</b>
	Vol*Benzene	<b>0</b>	<b>0</b>

# Gasoline Blending Example – Only Regular (Optimized)

<i>Raw Materials</i>	<i>Properties for Blending Calculations</i>							
	RON	MON	(R+M)/2	RVP	RVP <sup>1.25</sup>	Aromatics	Olefins	Benzene
Butane	93.0	92.0	92.5	54	146.4	0.0	0.0	0.00
Straight Run Naphtha	78.0	76.0	77	11.2	20.5	2.2	0.9	0.73
Isomerate	83.0	81.1	82.05	13.5	25.9	1.6	0.1	0.00
Reformate (High Octane)	100.0	88.2	94.1	3.2	4.3	94.2	0.6	1.85
Reformate (Low Benzene)	93.7	84.0	88.85	2.8	3.6	61.1	1.0	0.12
FCC Naphtha	92.1	77.1	84.6	1.4	1.5	35.2	32.6	1.06
Alkylate	97.3	95.9	96.6	4.6	6.7	0.5	0.2	0.00

	<i>Cost &amp; Availability</i>			<i>Usage</i>				
	Cost (\$/gal)	Minimum Required	Maximum Available	Regular	Premium	Total	Minimum Slack	Maximum Slack
Butane	<b>0.85</b>	<b>0</b>	<b>30,000</b>	<b>30,000</b>	<b>0</b>	30,000	<b>30,000</b>	<b>0</b>
Straight Run Naphtha	<b>2.05</b>	<b>0</b>	<b>35,000</b>	<b>35,000</b>	<b>0</b>	35,000	<b>35,000</b>	<b>0</b>
Isomerate	<b>2.20</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	0	<b>0</b>	<b>0</b>
Reformate (High Octane)	<b>2.80</b>	<b>0</b>	<b>60,000</b>	<b>12,628</b>	<b>0</b>	12,628	<b>12,628</b>	<b>47,372</b>
Reformate (Low Benzene)	<b>2.75</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	0	<b>0</b>	<b>0</b>
FCC Naphtha	<b>2.60</b>	<b>0</b>	<b>70,000</b>	<b>70,000</b>	<b>0</b>	70,000	<b>70,000</b>	<b>0</b>
Alkylate	<b>2.75</b>	<b>0</b>	<b>40,000</b>	<b>39,999</b>	<b>1</b>	40,000	<b>40,000</b>	<b>0</b>

<i>Products</i>		<i>Lower &amp; Upper Limits on Properties</i>	
		Lower	Upper
Regular	Octane	<b>87</b>	<b>110</b>
	RVP	<b>0.0</b>	<b>15.0</b>
	RVP <sup>1.25</sup>	0.0	29.5
Premium	Benzene	<b>0.0</b>	<b>1.1</b>
	Octane	<b>91</b>	<b>110</b>
	RVP	<b>0.0</b>	<b>15.0</b>
	RVP <sup>1.25</sup>	0.0	29.5
	Benzene	<b>0.0</b>	<b>1.1</b>

	<i>Price &amp; Production Requirements</i>		
	Price (\$/gal)	Minimum Required	Maximum Allowed
Regular	<b>2.75</b>	<b>1</b>	<b>1,000,000</b>
Premium	<b>2.85</b>	<b>1</b>	<b>1</b>

<i>Cost &amp; Revenue</i>			
Revenue (\$)	\$515,973	\$3	\$515,976
Cost(\$)	\$424,605	\$2	\$424,607
Profit (\$)	\$91,368	\$1	<b>\$91,369</b>

<i>Product Calculations</i>	<i>Volumes &amp; Properties</i>		
	Regular	Premium	Total
Produced	<b>187,627</b>	<b>1</b>	187,628
RON	91.25	91.75	
MON	84.03	90.25	
(R+M)/2	<b>87.6</b>	<b>91.0</b>	
RVP	<b>15.0</b>	<b>15.0</b>	
RVP <sup>1.25</sup>	29.52	29.52	
Benzene	<b>0.66</b>	<b>0.19</b>	

		<i>Linear-Form Product Constraints</i>	
		Lower Slack	Upper Slack
Regular	Volume	<b>187,626</b>	<b>812,373</b>
	Vol*Octane	<b>120,652</b>	<b>4,194,760</b>
	Vol*RVP <sup>1.25</sup>	<b>5,538,708</b>	<b>0</b>
Premium	Vol*Benzene	<b>123,111</b>	<b>83,278</b>
	Volume	<b>0</b>	<b>0</b>
	Vol*Octane	<b>0</b>	<b>19</b>
	Vol*RVP <sup>1.25</sup>	<b>30</b>	<b>0</b>
	Vol*Benzene	<b>0</b>	<b>1</b>

# Gasoline Blending Example – Only Premium (Optimized)

<i>Raw Materials</i>	<i>Properties for Blending Calculations</i>							
	RON	MON	(R+M)/2	RVP	RVP <sup>1.25</sup>	Aromatics	Olefins	Benzene
Butane	93.0	92.0	92.5	54	146.4	0.0	0.0	0.00
Straight Run Naphtha	78.0	76.0	77	11.2	20.5	2.2	0.9	0.73
Isomerate	83.0	81.1	82.05	13.5	25.9	1.6	0.1	0.00
Reformate (High Octane)	100.0	88.2	94.1	3.2	4.3	94.2	0.6	1.85
Reformate (Low Benzene)	93.7	84.0	88.85	2.8	3.6	61.1	1.0	0.12
FCC Naphtha	92.1	77.1	84.6	1.4	1.5	35.2	32.6	1.06
Alkylate	97.3	95.9	96.6	4.6	6.7	0.5	0.2	0.00

	<i>Cost &amp; Availability</i>			<i>Usage</i>				
	Cost (\$/gal)	Minimum Required	Maximum Available	Regular	Premium	Total	Minimum Slack	Maximum Slack
Butane	<b>0.85</b>	<b>0</b>	<b>30,000</b>	<b>0</b>	<b>30,000</b>	30,000	<b>30,000</b>	<b>0</b>
Straight Run Naphtha	<b>2.05</b>	<b>0</b>	<b>35,000</b>	<b>0</b>	<b>17,433</b>	17,433	<b>17,433</b>	<b>17,567</b>
Isomerate	<b>2.20</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	0	<b>0</b>	<b>0</b>
Reformate (High Octane)	<b>2.80</b>	<b>0</b>	<b>60,000</b>	<b>0</b>	<b>60,000</b>	60,000	<b>60,000</b>	<b>0</b>
Reformate (Low Benzene)	<b>2.75</b>	<b>0</b>	<b>0</b>	<b>0</b>	<b>0</b>	0	<b>0</b>	<b>0</b>
FCC Naphtha	<b>2.60</b>	<b>0</b>	<b>70,000</b>	<b>0</b>	<b>32,959</b>	32,959	<b>32,959</b>	<b>37,041</b>
Alkylate	<b>2.75</b>	<b>0</b>	<b>40,000</b>	<b>0</b>	<b>40,000</b>	40,000	<b>40,000</b>	<b>0</b>

<i>Products</i>		<i>Lower &amp; Upper Limits on Properties</i>	
		Lower	Upper
Regular	Octane	<b>87</b>	<b>110</b>
	RVP	<b>0.0</b>	<b>15.0</b>
	RVP <sup>1.25</sup>	0.0	29.5
	Benzene	<b>0.0</b>	<b>1.1</b>
Premium	Octane	<b>91</b>	<b>110</b>
	RVP	<b>0.0</b>	<b>15.0</b>
	RVP <sup>1.25</sup>	0.0	29.5
	Benzene	<b>0.0</b>	<b>1.1</b>

	<i>Price &amp; Production Requirements</i>		
	Price (\$/gal)	Minimum Required	Maximum Allowed
Regular	<b>2.75</b>	<b>1</b>	<b>1</b>
Premium	<b>2.85</b>	<b>1</b>	<b>1,000,000</b>

<i>Cost &amp; Revenue</i>			
Revenue (\$)	\$3	\$514,115	\$514,118
Cost(\$)	\$2	\$424,930	\$424,932
Profit (\$)	\$0	\$89,186	<b>\$89,186</b>

<i>Product Calculations</i>	<i>Volumes &amp; Properties</i>		
	Regular	Premium	Total
Produced	<b>1</b>	<b>180,391</b>	180,392
RON	90.90	94.67	
MON	83.10	87.33	
(R+M)/2	<b>87.0</b>	<b>91.0</b>	
RVP	<b>15.0</b>	<b>15.0</b>	
RVP <sup>1.25</sup>	29.52	29.52	
Benzene	<b>1.10</b>	<b>0.88</b>	

		<i>Linear-Form Product Constraints</i>	
		Lower Slack	Upper Slack
Regular	Volume	<b>0</b>	<b>0</b>
	Vol*Octane	<b>0</b>	<b>23</b>
	Vol*RVP <sup>1.25</sup>	<b>30</b>	<b>0</b>
	Vol*Benzene	<b>1</b>	<b>0</b>
Premium	Volume	<b>180,390</b>	<b>819,609</b>
	Vol*Octane	<b>0</b>	<b>3,427,436</b>
	Vol*RVP <sup>1.25</sup>	<b>5,325,125</b>	<b>0</b>
	Vol*Benzene	<b>158,662</b>	<b>39,769</b>



# Gasoline Blending Example – Combined (Optimized)

<i>Raw Materials</i>	<i>Properties for Blending Calculations</i>							
	RON	MON	(R+M)/2	RVP	RVP <sup>1.25</sup>	Aromatics	Olefins	Benzene
Butane	93.0	92.0	92.5	54	146.4	0.0	0.0	0.00
Straight Run Naphtha	78.0	76.0	77	11.2	20.5	2.2	0.9	0.73
Isomerate	83.0	81.1	82.05	13.5	25.9	1.6	0.1	0.00
Reformate (High Octane)	100.0	88.2	94.1	3.2	4.3	94.2	0.6	1.85
Reformate (Low Benzene)	93.7	84.0	88.85	2.8	3.6	61.1	1.0	0.12
FCC Naphtha	92.1	77.1	84.6	1.4	1.5	35.2	32.6	1.06
Alkylate	97.3	95.9	96.6	4.6	6.7	0.5	0.2	0.00

	<i>Cost &amp; Availability</i>			<i>Usage</i>				
	Cost (\$/gal)	Minimum Required	Maximum Available	Regular	Premium	Total	Minimum Slack	Maximum Slack
Butane	0.85	0	30,000	17,925	12,075	30,000	30,000	0
Straight Run Naphtha	2.05	0	35,000	35,000	0	35,000	35,000	0
Isomerate	2.20	0	0	0	0	0	0	0
Reformate (High Octane)	2.80	0	60,000	43,599	16,401	60,000	60,000	0
Reformate (Low Benzene)	2.75	0	0	0	0	0	0	0
FCC Naphtha	2.60	0	70,000	24,226	45,774	70,000	70,000	0
Alkylate	2.75	0	40,000	0	40,000	40,000	40,000	0

<i>Products</i>		<i>Lower &amp; Upper Limits on Properties</i>	
		Lower	Upper
Regular	Octane	87	110
	RVP	0.0	15.0
	RVP <sup>1.25</sup>	0.0	29.5
Premium	Benzene	0.0	1.1
	Octane	91	110
	RVP	0.0	15.0
	RVP <sup>1.25</sup>	0.0	29.5
	Benzene	0.0	1.1

	<i>Price &amp; Production Requirements</i>		
	Price (\$/gal)	Minimum Required	Maximum Allowed
Regular	2.75	1	1,000,000
Premium	2.85	1	1,000,000

<i>Cost &amp; Revenue</i>			
Revenue (\$)	\$332,063	\$325,613	\$657,675
Cost(\$)	\$272,051	\$285,199	\$557,250
Profit (\$)	\$60,011	\$40,414	<b>\$100,425</b>

	<i>Product Calculations</i>		
	<i>Volumes &amp; Properties</i>		
	Regular	Premium	Total
Produced	120,750	114,250	235,000
RON	91.00	95.15	
MON	83.00	86.85	
(R+M)/2	87.0	91.0	
RVP	15.0	10.6	
RVP <sup>1.25</sup>	29.52	19.05	
Benzene	1.09	0.69	

		<i>Linear-Form Product Constraints</i>	
		Lower Slack	Upper Slack
Regular	Volume	120,749	879,250
	Vol*Octane	0	2,777,250
	Vol*RVP <sup>1.25</sup>	3,564,521	0
Premium	Vol*Benzene	131,888	937
	Volume	114,249	885,750
	Vol*Octane	0	2,170,750
	Vol*RVP <sup>1.25</sup>	2,176,967	1,195,675
	Vol*Benzene	78,862	46,813

# Gasoline Blending Example – Lower RVP & Benzene

<i>Raw Materials</i>	<i>Properties for Blending Calculations</i>							
	RON	MON	(R+M)/2	RVP	RVP <sup>1.25</sup>	Aromatics	Olefins	Benzene
Butane	93.0	92.0	92.5	54	146.4	0.0	0.0	0.00
Straight Run Naphtha	78.0	76.0	77	11.2	20.5	2.2	0.9	0.73
Isomerate	83.0	81.1	82.05	13.5	25.9	1.6	0.1	0.00
Reformat (High Octane)	100.0	88.2	94.1	3.2	4.3	94.2	0.6	1.85
Reformat (Low Benzene)	93.7	84.0	88.85	2.8	3.6	61.1	1.0	0.12
FCC Naphtha	92.1	77.1	84.6	1.4	1.5	35.2	32.6	1.06
Alkylate	97.3	95.9	96.6	4.6	6.7	0.5	0.2	0.00

	<i>Cost &amp; Availability</i>			<i>Usage</i>				
	Cost (\$/gal)	Minimum Required	Maximum Available	Regular	Premium	Total	Minimum Slack	Maximum Slack
Butane	0.85	0	30,000	8,187	0	8,188	8,188	21,812
Straight Run Naphtha	2.05	0	35,000	28,305	0	28,305	28,305	6,695
Isomerate	2.20	0	0	0	0	0	0	0
Reformat (High Octane)	2.80	0	60,000	0	0	0	0	60,000
Reformat (Low Benzene)	2.75	0	0	0	0	0	0	0
FCC Naphtha	2.60	0	70,000	60,824	0	60,824	60,824	9,176
Alkylate	2.75	0	40,000	40,000	0	40,000	40,000	0

<i>Products</i>		<i>Lower &amp; Upper Limits on Properties</i>	
		Lower	Upper
Regular	Octane	87	110
	RVP	0.0	9.0
	RVP <sup>1.25</sup>	0.0	15.6
Premium	Benzene	0.0	0.62
	Octane	91	110
	RVP	0.0	9.0
	RVP <sup>1.25</sup>	0.0	15.6
	Benzene	0.0	0.62

	<i>Price &amp; Production Requirements</i>		
	Price (\$/gal)	Minimum Required	Maximum Allowed
Regular	2.75	1	1,000,000
Premium	2.85	1	1,000,000

<i>Cost &amp; Revenue</i>			
Revenue (\$)	\$377,618	\$3	\$377,621
Cost(\$)	\$333,125	\$3	\$333,127
Profit (\$)	\$44,493	\$0	\$44,493

	<i>Product Calculations</i>		
	<i>Volumes &amp; Properties</i>		
	Regular	Premium	Total
Produced	137,316	1	137,317
RON	90.76	95.03	
MON	83.24	86.97	
(R+M)/2	87.0	91.0	
RVP	9.0	9.0	
RVP <sup>1.25</sup>	15.59	15.59	
Benzene	0.62	0.62	

		<i>Linear-Form Product Constraints</i>	
		Lower Slack	Upper Slack
Regular	Volume	137,315	862,684
	Vol*Octane	0	3,158,261
	Vol*RVP <sup>1.25</sup>	2,140,540	0
Premium	Vol*Benzene	85,136	0
	Volume	0	999,999
	Vol*Octane	0	19
	Vol*RVP <sup>1.25</sup>	16	0
	Vol*Benzene	1	0

# Gasoline Blending Example –Low Benzene Reformate

<i>Raw Materials</i>	<i>Properties for Blending Calculations</i>							
	RON	MON	(R+M)/2	RVP	RVP <sup>1.25</sup>	Aromatics	Olefins	Benzene
Butane	93.0	92.0	92.5	54	146.4	0.0	0.0	0.00
Straight Run Naphtha	78.0	76.0	77	11.2	20.5	2.2	0.9	0.73
Isomerate	83.0	81.1	82.05	13.5	25.9	1.6	0.1	0.00
Reformate (High Octane)	100.0	88.2	94.1	3.2	4.3	94.2	0.6	1.85
Reformate (Low Benzene)	93.7	84.0	88.85	2.8	3.6	61.1	1.0	0.12
FCC Naphtha	92.1	77.1	84.6	1.4	1.5	35.2	32.6	1.06
Alkylate	97.3	95.9	96.6	4.6	6.7	0.5	0.2	0.00

	<i>Cost &amp; Availability</i>			<i>Usage</i>				
	Cost (\$/gal)	Minimum Required	Maximum Available	Regular	Premium	Total	Minimum Slack	Maximum Slack
Butane	0.85	0	30,000	13,552	1,355	14,907	14,907	15,093
Straight Run Naphtha	2.05	0	35,000	35,000	0	35,000	35,000	0
Isomerate	2.20	0	0	0	0	0	0	0
Reformate (High Octane)	2.80	0	0	0	0	0	0	0
Reformate (Low Benzene)	2.75	0	65,400	53,656	11,744	65,400	65,400	0
FCC Naphtha	2.60	0	70,000	70,000	0	70,000	70,000	0
Alkylate	2.75	0	40,000	35,854	4,146	40,000	40,000	0

<i>Products</i>		<i>Lower &amp; Upper Limits on Properties</i>	
		Lower	Upper
Regular	Octane	87	110
	RVP	0.0	9.0
	RVP <sup>1.25</sup>	0.0	15.6
	Benzene	0.0	0.62
Premium	Octane	91	110
	RVP	0.0	9.0
	RVP <sup>1.25</sup>	0.0	15.6
	Benzene	0.0	0.62

	<i>Price &amp; Production Requirements</i>		
	Price (\$/gal)	Minimum Required	Maximum Allowed
Regular	2.75	1	1,000,000
Premium	2.85	1	1,000,000

<i>Cost &amp; Revenue</i>			
Revenue (\$)	\$572,172	\$49,147	\$621,318
Cost(\$)	\$511,423	\$44,848	\$556,271
Profit (\$)	\$60,749	\$4,299	\$65,048

	<i>Product Calculations</i>		
	<i>Volumes &amp; Properties</i>		
	Regular	Premium	Total
Produced	208,062	17,244	225,307
RON	91.10	94.51	
MON	82.90	87.49	
(R+M)/2	87.0	91.0	
RVP	9.0	9.0	
RVP <sup>1.25</sup>	15.59	15.59	
Benzene	0.51	0.08	

		<i>Linear-Form Product Constraints</i>	
		Lower Slack	Upper Slack
Regular	Volume	208,061	791,938
	Vol*Octane	0	4,785,436
	Vol*RVP <sup>1.25</sup>	3,243,372	0
	Vol*Benzene	106,189	22,810
Premium	Volume	17,243	982,756
	Vol*Octane	0	327,645
	Vol*RVP <sup>1.25</sup>	268,815	0
	Vol*Benzene	1,409	9,282

# Adjusting operations to meet targets

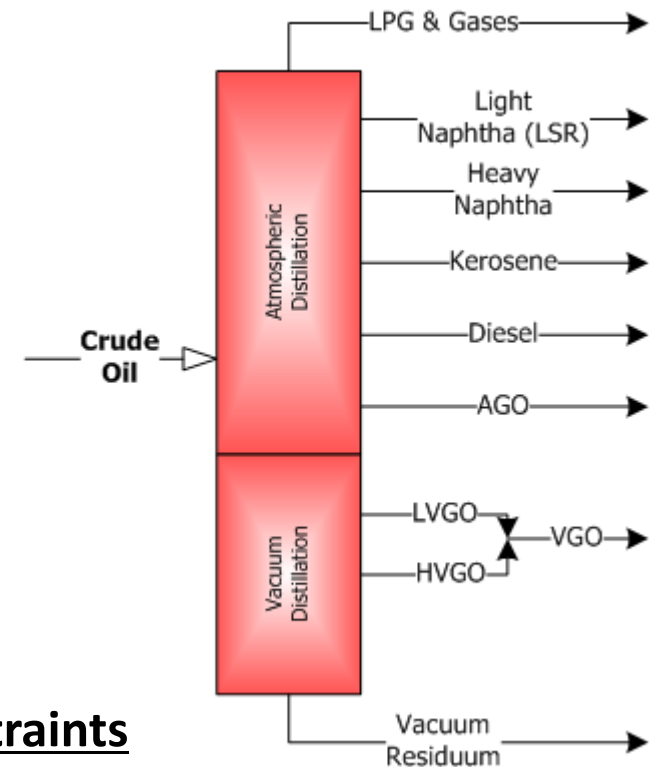
Updated: July 12, 2018  
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# Cutpoint Economics

Adjust upstream cutpoints to meet needs in the downstream blending

- Heavy LSR...value as blending component versus Reformer feed
- Heavy Naphtha...value as Reformer feed versus kerosene blend stock
- Heavy Kerosene...value as kerosene blend stock versus diesel blend stock
- Heavy Diesel...value as diesel blend stock versus FCC feed
- Heavy Gas Oil...value as FCC feed versus resid/asphalt production or coker feed

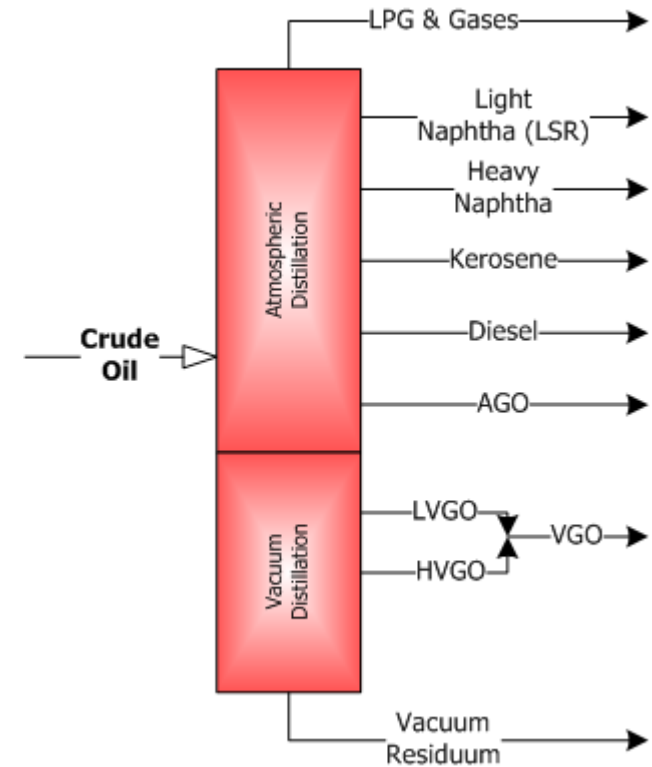
**The refinery LP can determine the optimum cut point for each of these given any set of constraints**



# Cutpoints To Meet Operating Economies

TBP Cut Points (°F) for Various Crude Oil Fractions

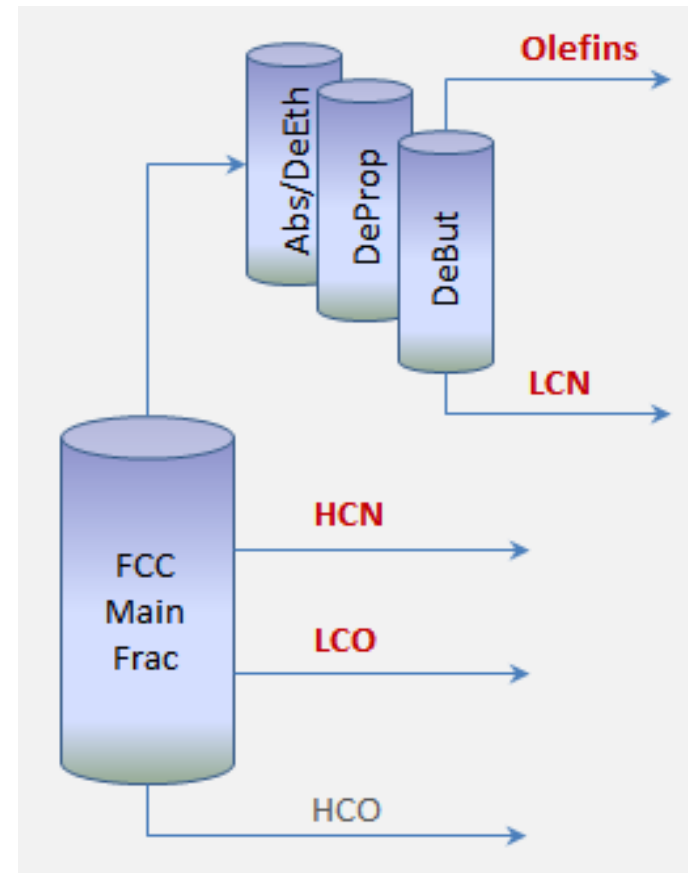
Cut	IBP	EP	Processing Use
LSR	90	180	Min LSR cut
	90	190	Normal LSR cut
	80	220	Max LSR cut
Naphtha	180	380	Max reforming cut
	190	330	Max jet fuel
	220	330	Min reforming cut
Kerosene	330	520	Max kerosene cut
	330	480	Max Jet A cut
	380	520	Max gasoline
Diesel	420	650	Max diesel cut
	480	610	Max jet fuel cut
	520	610	Min diesel cut
Gas Oil	610	800	Cat cracker feed
VGO	800	1050	Cat cracker feed
Resid	1050+		Coker feed, asphalt



# Optimize FCC Gasoline Distillation

## Frame the analysis

- What is the value of the molecules in the ***stream above***?
- What is the value of the molecules in the ***stream below***?
- What ***upstream unit*** operations affect the stream value?
- What ***downstream unit*** operations affect the stream value?
- What ***unit specific*** operations affect the stream value?
- What ***product blending*** constraints affect the stream value?



Ref: [http://www.refinerlink.com/blog/Truly\\_Optimize\\_FCC\\_Gasoline\\_Distillation](http://www.refinerlink.com/blog/Truly_Optimize_FCC_Gasoline_Distillation)

# Optimize FCC Gasoline Distillation

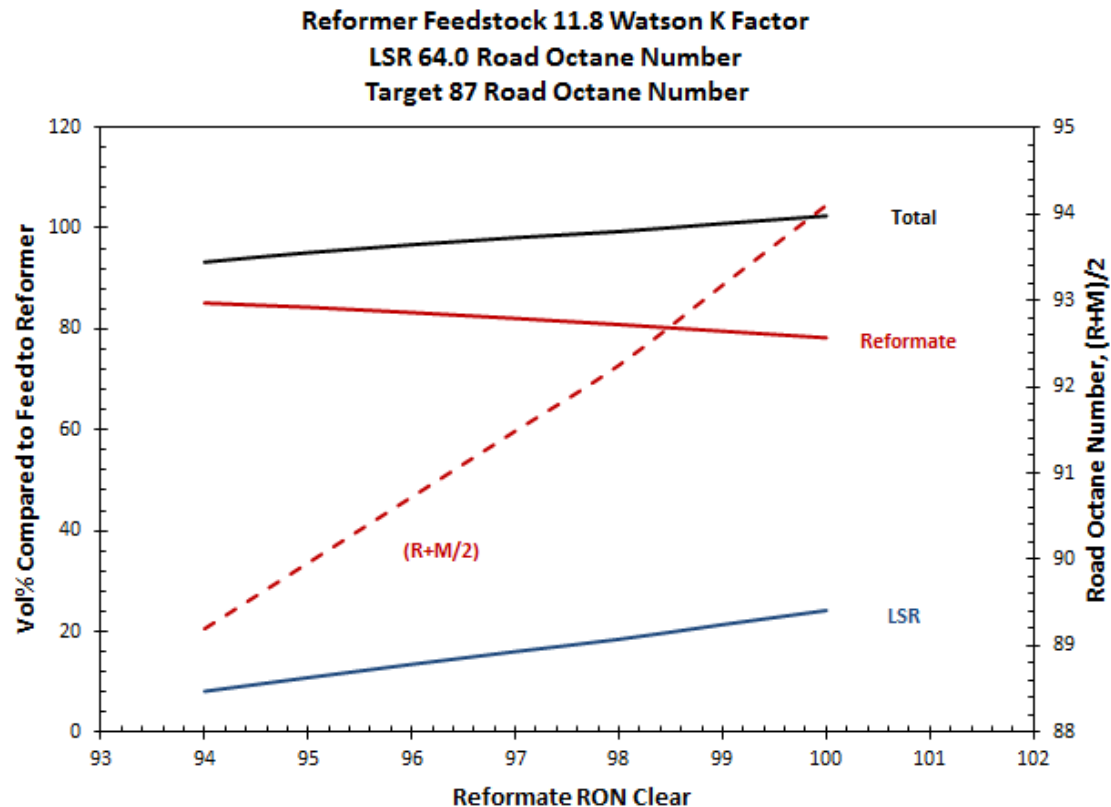
	LCN	HCN
Value to the <b>stream above</b> ?	<p>May have sub-optimal amount of olefins:</p> <ul style="list-style-type: none"> <li>Alkylation unit downstream have capacity for the olefins?</li> <li>Type of alky unit? Sulfuric Alky can take more C5= olefins; HF Alky limited by strength concerns</li> <li>Time of year? Alky economics better during summer</li> </ul>	When distillate more valuable than gasoline minimize the LCN/HCN cut point to maximize distillate production from HCN
Value to the <b>stream below</b> ?	When distillate more valuable than gasoline minimize the LCN/HCN cut point to maximize distillate production from HCN contributions	<p>Diesel prices higher than gasoline, minimize HCN end point &amp; still make diesel flash limit</p> <p>If LCO is routed to a Hydrocracker HCN end point can be adjusted to make jet flash limit.</p> <p>HCN endpoint can also be used to optimize heavy fuel oil blending when LCO is used as a cutter</p>
<b>Upstream unit</b> affects?	Degree of hydrotreating possible to give low sulfur content in final product	Degree of hydrotreating possible to give low sulfur content in final product
<b>Downstream unit</b> affects?	<p>Destination of LCN?</p> <ul style="list-style-type: none"> <li>Gasoline Hydrotreater &amp; then to blend pool</li> <li>Selective Hydrogenation Unit &amp; then to Reformer</li> </ul> <p>High olefin content will increase hydrogen requirements in downstream hydrotreaters</p>	<p>If routed to Gasoline Hydrotreater may reduce end point to better make gasoline sulfur specs</p> <p>If routed to Jet Hydrotreater then make-up hydrogen constraints may limit end point</p>
<b>Unit specific</b> affects?	<p>Subtle constraints such as olefin content and octane value will be influenced by a combination of riser and distillation targets.</p> <p>Cat-to-oil ratio affects product mix, thus distillation strategies.</p>	Fractionator draw constraints may be handled by adjusting FCC reactor conditions & yields
<b>Product blending</b> constraints?	Usually routed to gasoline – need to olefins, sulfur, and aromatics	<p>When routing to gasoline, use HCN endpoint to adjust gasoline sulfur, endpoint, and aromatics.</p> <p>When routing to jet, use HCN IBP to meet jet flash &amp; endpoint to manage jet freeze &amp; smoke point.</p> <p>When routing to diesel, use IBP to manage diesel flash</p>

Ref: [http://www.refinerlink.com/blog/Truly\\_Optimize\\_FCC\\_Gasoline\\_Distillation](http://www.refinerlink.com/blog/Truly_Optimize_FCC_Gasoline_Distillation)



# Gasoline Blending – Modify Upstream Operations

How much gasoline can be produced by blending Reformate+LSR with respect to the Reformer's severity?



# General Gasoline Blending Considerations

## Reduce RVP giveaway

- Blend nC4, not iC4.
  - iC4 has higher vapor pressure than nC4
  - iC4 has more value as alkylation feedstock

## Reduce Octane giveaway

- Setting constant reformer severity target – hydrogen & octane balance highly dynamic constraints
- Blending low octane components to reduce octane giveaway – maybe there's just too much high octane blendstock?

[http://www.refinerlink.com/blog/Redefining\\_Gasoline\\_RVP\\_Giveaway](http://www.refinerlink.com/blog/Redefining_Gasoline_RVP_Giveaway)  
[http://www.refinerlink.com/blog/Top\\_3\\_Refinery\\_Octane\\_Blending\\_Mistakes/](http://www.refinerlink.com/blog/Top_3_Refinery_Octane_Blending_Mistakes/)

# General Gasoline Blending Considerations

Many blending problems require fixes to upstream operations

- RVP

- Poor depropanizer operation allowing propane into the butane pool?
- Proper splitting in Deisobutanizer & isostrippers?

- Octane

- Correct cut points between heavy naphtha & kerosene?
- Reduce reformer severity?
  - May not be possible if hydrogen needed.
- Batch operating reformer severity?
  - Would provide balance between octane enhancement & volume to blending
- Reducing reformer feed rates
- Selling high octane components

[http://www.refinerlink.com/blog/Redefining\\_Gasoline\\_RVP\\_Giveaway](http://www.refinerlink.com/blog/Redefining_Gasoline_RVP_Giveaway)  
[http://www.refinerlink.com/blog/Top\\_3\\_Refinery\\_Octane\\_Blending\\_Mistakes/](http://www.refinerlink.com/blog/Top_3_Refinery_Octane_Blending_Mistakes/)

# Summary

Updated: July 12, 2018  
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# Summary

Equations for the blending of intermediate stocks to meet final product specifications

Equation forms have been developed to be used with optimization tools (such as linear programming)

Proper optimization of a facility will include adjusting upstream operations to meet downstream targets